NAVAL POSTGRADUATE SCHOOL MONTEREY CA F/G 9/2 USE OF THE TI 59 WITH APPLICATIONS TO PROBABILITY AND STATISTIC--ETC(U) DEC 80 G R NELSON, E E STANTON AD-A097 384 MINCLASSIFIED NL 1 in 2 40 4097464

LIELI



NAVAL POSTGRADUATE SCHOOL

Monterey, California



DTIC ELECTE APR7 1981

Tipod > 20 THESIS

USE OF THE TI 59 WITH APPLICATIONS TO
PROBABILITY AND STATISTICAL ANALYSIS •

by

George Russell/Nelson

Edgar Emmett Stanton III

December 180

P. W. Zehna

Thesis Advisor:

Approved for public release; distribution unlimited

TE FILE COPY

AD A 0 9738

81 4 8 061 21 115 p

# SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM		
REPORT NUMBER		3. RECIPIENT'S CATALOG NUMBER		
TITLE (and Subtitio)		S. TYPE OF REPORT & PERIOD COVERE		
Use of the TI 59 with Applica	tions	Master's Thesis;		
to Probability and Statistical A		(December 1980)		
•	•	6. PERFORMING ORG. REPORT NUMBER		
AUTHOR(a)	<del></del>	8. CONTRACT OR GRANT NUMBER(s)		
George Russell Nelson				
Edgar Emmett Stanton III				
PERFORMING ORGANIZATION NAME AND ADDRES				
		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS		
Naval Postgraduate School				
Monterey, California 93940	•			
CONTROLLING OFFICE HAME AND ADDRESS	·	12. REPORT DATE		
Naval Postgraduate School		December 1980		
Monterey, California 93940	•	13. NUMBER OF PAGES		
• • • • • • • • • • • • • • • • • • • •		161		
Moniforing Adency NAME & ADDRESSIO Miles Naval Postgraduate School	ent from Controlling Office)	18. SECURITY CLASS. (of this report)		
"ALCT TOO PERSON DCDOOL				
Monterey, California 93940		Unclassified		
		Unclassified  18a. GECLASSIFICATION/DOWNGRAGING SCHEDULE		
Monterey, California 93940  DISTRIBUTION STATEMENT (of this Report)		ISA. DECLASSIFICATION/DOWNGRADING		
Monterey, California 93940		ISA. DECLASSIFICATION/DOWNGRADING		
Monterey, California 93940  DISTRIBUTION STATEMENT (of this Report)		ISA. DECLASSIFICATION/DOWNGRADING		
Monterey, California 93940  DISTRIBUTION STATEMENT (of this Report)		ISA. DECLASSIFICATION/DOWNGRADING		
Monterey, California 93940  DISTRIBUTION STATEMENT (of this Report)	e; distribution u	ISA. DECLASSIFICATION/DOWNGRADING SCHEDULE		
Monterey, California 93940  DISTRIBUTION STATEMENT (of this Report)  Approved for public releas	e; distribution u	ISA. DECLASSIFICATION/DOWNGRADING SCHEDULE		
Monterey, California 93940  DISTRIBUTION STATEMENT (of this Report)  Approved for public releas	e; distribution w	ISO. OECLASSIFICATION/DOWNGRAGING SCHEDULE nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (et this Report)  Approved for public releas  DISTRIBUTION STATEMENT (et the abetrest entere	e; distribution w	ISO. OECLASSIFICATION/DOWNGRAGING SCHEDULE nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (et this Report)  Approved for public releas  Approved for public releas	e; distribution w	ISO. OECLASSIFICATION/DOWNGRAGING SCHEDULE nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (et this Report)  Approved for public releas  DISTRIBUTION STATEMENT (et the abetrest entere	e; distribution w	ISO. OECLASSIFICATION/DOWNGRAGING SCHEDULE nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (et this Report)  Approved for public releas  Approved for public releas	e; distribution w	ISO. OECLASSIFICATION/DOWNGRAGING SCHEDULE nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (et this Report)  Approved for public releas  Approved for public releas	e; distribution w	ISO. OECLASSIFICATION/DOWNGRAGING SCHEDULE nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (et this Report)  Approved for public releas  Approved for public releas	e; distribution w	ISO. OECLASSIFICATION/DOWNGRAGING SCHEDULE nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (et this Report)  Approved for public releas  Approved for public releas	e; distribution was a second for all section of the second for the	ISA. OECLASSIFICATION/DOWNDRAGING nlimited  m. Report) nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (of the obstract entered  Approved for public releas  Approved for public releas  SUPPLEMENTARY NOTES	e; distribution was a second for all section of the second for the	ISA. OECLASSIFICATION/DOWNDRAGING nlimited  m. Report) nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (of the Report)  Approved for public releas  Approved for public releas  SUPPLEMENTARY NOTES	e; distribution was a second for all section of the second for the	ISA. OECLASSIFICATION/DOWNDRAGING nlimited  m. Report) nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (of the Report)  Approved for public releas  Approved for public releas  Supplementary notes  KEY WORDS (Continue on reverse olds if necessary of TI 59 Use	e; distribution was a second for all section of the second for the	ISA. OECLASSIFICATION/DOWNDRAGING nlimited  m. Report) nlimited		
Monterey, California 93940  DISTRIBUTION STATEMENT (of the Report)  Approved for public releas  Approved for public releas  Supplementary notes  KEY WORDS (Continue on reverse side if necessary of TI 59 Use TI 59 Simulation	e; distribution was a second for all section of the second for the	ISA. OECLASSIFICATION/DOWNDRAGING nlimited  m. Report) nlimited		

This thesis demonstrates through three comprehensive examples, the capabilities of the TI 59 programmable hand-held calculator as an analytical tool. Cne example is a probability application while the other two examples entail use of the TI 59 in statistical inference and data analysis. The probability example involves the use of the Monte Carlo technique to simulate stochastically the detection, identification and engagement of a cruise missile by an Improved Hawk Air Defense Battery.

DD | FORM 1473 EDITION OF 1 NOV 68 IS OBSOLETE S/N 0102-014-6601 |

Unclassified

PEUMTY CLASSIFICATION OF THIS PAGE/THE Rose Entere

The second example illustrates a TI 59 program which is designed to analyze sample data. The data used for this illustration were gathered by the authors in an experiment which encompassed the testing of thirty-six male subjects to determine the extent to which their training routines influenced their strength, endurance, and cardiovascular fitness. The third example involves the use of an ANOVA routine and Scheffe's multiple contrasts to demonstrate how the TI 59 may be used to facilitate statistical inferences. The fitness data are also used for this purpose. The intent throughout the thesis is to exemplify the capabilities of the TI 59 as a viable, real world analytical tool rather than emphasize particular results of the simulation or the experiment.

Anos,	
1.7	$\boldsymbol{\times}$
	fightion
By	And the f
	ibution/ lability Obdes
- AVAI	Avail ann/or
Dist	Special
1	
111	1
1	l

# Approved for public release; distribution unlimited

Use of the TI 59 with Applications to Probability and Statistical Analysis

by

George Russell Nelson Captain, United States Army B.S., Ohio State University, 1971

Edgar Emmett Stanton III Captain, United States Army B.S., Florida State University, 1972

Submitted in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE IN MANAGEMENT

Approved by:

Chairman Department of Administrative Science

The Science School APR 7 19

Chairman Department of Administrative Science

Dean of Information and Policy Sciences

#### ABSTRACT

This thesis demonstrates through three comprehensive examples, the capabilities of the TI 59 programmable hand-held calculator as an analytical tool. One example is a probability application while the other two examples entail use of the TI 59 in statistical inference and data analysis. The probability example involves the use of the Monte Carlo technique to simulate stochastically the detection, identification and engagement of a cruise missile by an Improved Hawk Air Defense Battery. The second example illustrates a TI 59 program which is designed to analyze sample data. The data used for this illustration were gathered by the authors in an experiment which encompassed the testing of thirty-six male subjects to determine the extent to which their training routines influenced their strength, endurance, and cardiovascular fitness. The third example involves the use of an ANOVA routine and Scheffe's multiple contrasts to demonstrate how the TI 59 may be used to facilitate statistical inferences. The fitness data are also used for this purpose. The intent throughout the thesis is to exemplify the capabilities of the TI 59 as a viable, real world analytical tool rather than emphasize particular results of the simulation or the experiment.

# TABLE OF CONTENTS

I.	INTRODUCTION		
II.	PRO	DBABILITY 1	LO
	A.	MONTE CARLO TECHNIQUE	Ll
	в.	TI 59 RANDOM NUMBER GENERATOR	L2
		1. Uniform Random Number Generator 1	<u>.</u> 4
		2. Norma Random Number Generator 1	.6
		3. SBR 2nd D.MS 1	.8
	c.	COMBAT MODELS 1	.9
III.	COM	BAT SIMULATION USING TI 59	30
	Α.	IHAWK SYSTEM	31
		1. Detection 3	31
		2. Identification 3	34
		3. Engagement/Destruction	36
		4. Target 3	38
		5. Time 3	39
	В.	MACRO FLOWCHART	9
	c.	MICRO FLOWCHART 4	4
	D.	SUBROUTINES, LABELS, FLAGS, DATA REGISTERS AND PROGRAM MEMORY STEPS4	4
		1. Subroutines and Labels 4	4
		2. Flags 4	4
		3. Data Registers 4	۶۶
		4. Program Memory Steps	16

	E.	USER INSTRUCTIONS	47
		1. Step 2 Clear Data Registers	47
		2. Step 9 Check Data Register Content	47
	F.	SENSITIVITY ANALYSIS RESULTS FOR LOCK-ON TIMES	47
	G.	RECOMMENDATIONS	48
IV.	DAT	A ANALYSIS	57
	A.	PURPOSE	57
	В.	FITNESS EXPERIMENT	57
		1. Scope of the Experiment	57
		2. Experimental Design	59
		3. Scoring Methodology	63
		4. Test Results	64
	C.	TI 59 PROGRAM FOR DATA ANALYSIS	64
		1. TI 59 Capabilities	65
		2. Univariate Data Program	66
	D.	APPLICATION OF THE TI 59 UNIVARIATE PROGRAM	69
ν.	STA	TISTICAL INFERENCE	83
	Α.	PURPOSE	83
	В.	TI 59 PROGRAM FOR ANALYSIS OF VARIANCE	83
	C.	APPLICATION OF THE TI 59 ANOVA PROGRAM	88
	D.	SUMMARY	92
APPEN	DIX	A Simulation Labels, Program and Micro Flowchart	102
APPEN	DIX	B Physical Fitness Test Questionnaire and Data Forms.	119
LIST	OF R	EFERENCES	160
INITI	AL I	DISTRIBUTION LIST	161

### ACKNOWLEDGEMENTS

We wish to express our gratitude to several people for their invaluable assistance in the completion of this thesis. We thank Professor Peter W. Zehna for his didactic guidance and personal concern. We also wish to thank our wives, Jo Anne and Paula for their arduous efforts in the editing and typing of the manuscript. More importantly, we wish to recognize the love and support of our families that made this effort possible.

### I. INTRODUCTION

The intent of this thesis is do demonstrate through three comprehensive examples, the tremendous capabilities of the TI 59 programmable hand-held calculator. One of the examples is a probability application while the other two entail use of the TI 59 in statistical inference and data analysis.

The example chosen to illustrate an application to probability theory is a combat simulation model. The model involves use of the Monte Carlo technique to simulate stochastically detection, identification, and engagement of a cruise missile by an Improved Hawk Air Defense Battery. Chapter III discusses the combat model and the TI 59 simulation in detail. Chapter II addresses briefly the Monte Carlo technique, combat modeling in general, and the TI 59 random number generator in order that the reader may better understand the combat model discussed in Chapter III.

Two examples are provided for statistical applications of the calculator. These involve the analysis of data gathered by the authors in a physical fitness experiment. The experiment, discussed in detail in Chapter IV, involved the testing of thirty-six male subjects who were divided into six categories based on their training routine, to determine whether the subjects' training program did in fact influence their physical fitness. Chapter IV describes the fitness experiment in terms of its scope, design and scoring methodology. Chapter IV also discusses a TI 59 program which computes measures of central tendency and spread and then illustrates the use of the program with the fitness data.

Chapter V describes a TI 59 program for analysis of variance and then demonstrates how the program may be used with fitness data to make statistical inferences.

Throughout the thesis, it is assumed that the reader is generally familiar with programming techniques for the TI 59 hand-held calculator. Subroutines, labels, flags, data registers, and program steps are discussed in each of the ensuing chapters where the intent is to illustrate how the features of the calculator may be exploited to facilitate statistical analysis or simulation. Reference 12 discusses programming techniques for the TI 59. The TI 59 has one particular feature which makes it much more than a calculator. Specifically the capacity to use subroutines provides a analytical tool more like a minicomputer than a calculator. The three programs discussed in the succeeding chapters use subroutines extensively to illustrate this powerful capability.

Finally, while a few of the referenced tables and charts of this thesis are positioned close to comments discussing their purpose, most are to be found at the conclusion of each chapter or in the appendices.

### II. PROBABILITY

The intention of the authors was to begin this chapter discussion with a definition of probability theory, that branch of mathematics generally believed to have been founded by a Swiss mathematician named Jacques Bernoulli. However, research has revealed that there is some discussion as to the true meaning of probability theory and that among mathematicians there appear to be those who view probability as a state of the universe while others consider probability a state of belief. To compound this situation furthermore, there appear to be differing definitions of probability within each group. Indeed, all attempts to define probability directly have failed to meet with success. Instead, probability has been axiomitized, much like geometry, so that a set of consistency rules or axioms established by A. Kolmogorov are now generally accepted by the scientific community. These axioms allow a great deal of freedom in the assignment of probabilities for any particular model and at the same time force any such assignment to be consistent with any other. Moreover, the theorems of that theory then become universally true statements for any such assignment. In this system, events are defined as sets in a specified sample space. With those guidelines as a background, probability theory can be used to make intelligent predictions and decisions if we know what events are possible and how probable are the various events. After a little thought it becomes immediately apparent that the immense power of such a tool as probability theory is limited in use only by one's imagination and

ingenuity. This research is an effort to use probability theory in the construction of a probabilistic combat simulation on the Texas Instruments programmable 59 calculator (TI 59). Because the simulation developed includes a number of the many chance elements involved in most combat situations, a discussion of the Monte Carlo technique and random number generation on the TI 59 follows. A brief disussion of combat model simulations concludes this chapter.

#### A. MONTE CARLO TECHNIQUE

Systems that exhibit stochastic elements in their behavior can be simulated with the aid of the technique called Monte Carlo (named after the famous gambling resort town of Monaco). This technique involves sampling from those known probability distributions that represent each of the actual chance processes included in the system under study [Ref. 9]. By completing a system simulation run many times while keeping the non-stochastic inputs constant but allowing the chance elements to fluctuate according to their known probability distributions, a statistical average for run results can be determined.

Turban and Meredith Ref. 8 have listed the steps necessary in building a Monte Carlo simulation as follows:

- "1. Describe the system and obtain the probability distributions of the relevant probabilistic elements of the system.
- 2. Define the appropriate measure(s) of performance.
- Construct cumulative probability distributions for each of the stochastic elements.
- 4. Assign representative numbers in correspondence with the cumulative probability distributions.
- 5. Generate a random number for each of the independent stochastic elements and . . . (determine) the measure of system performance.
- Repeat step five until the measure of system performance stabilizes."

Thus the distinguishing feature of the Monte Carlo method is the repetitive execution of an established experiment or simulation involving
randomness.

While electronic digital computers themselves are not necessary for the execution of simulations, they do offer tremendous speed and consistency of conditions for such models. Thus the computer is ideally suited to perform the large number of repetitions required by Monte Carlo but the matter of landomness presents a problem. For the Monte Carlo technique described above the necessity of a truly random number is essential. However Kovach Ref. 6 notes that:

"Strictly speaking, the random number exists only as the result of a random process."

While computers, to include the TI 59, do possess the capacity to continuously generate random numbers as they are needed, these numbers are subject to the limitations of the computer and are not truly the result of a random process and hence are often described as pseudo-random.

### B. TI 59 RANDOM NUMBER GENERATOR

R.F. Barton [Ref. 4] describes simulation as follows:

"Simulation is simply the dynamic execution or manipulation of a model of an object system for some purpose.

Simulation is a case-by-case method for studying object systems. Each case might be either a single trial or an entire run. In either view, outputs may differ trial to trial and run to run."

The object system is that system under study in the simulation.

The TI 59 in its capacity as an electronic computer provides the user with the means of developing and executing stochastic and nonstochastic simulations.

Barton continues Ref. 4 :

" A stochastic simulation is one in which differing outputs trial to trial can be obtained without changing the inputs (ignoring random numbers as inputs). Specifically, this means that identical parameters, starting conditions, and input time path values produce varying outputs trial to trial and run to run.

A nonstochastic simulation is one in which the inputs or the model must be changed to obtain changed outputs. This means that identical model operations, parameters, starting conditions, and input time path values will produce identical outputs run to run. "

There are inputs common to both of these simulation types. However, as alluded to above, there are also special inputs that are needed to represent the chance processes or stochastic events found only within a stochastic simulation. These special inputs are random numbers.

The characteristic of random numbers that makes them different from all other numbers is the fact that the knowledge of any future random number cannot be enhanced by the knowledge of any past, present, or other future random number.

The TI 59 with its master library module solid state software program ML-15, a random number generator, can generate sequences of uniformly or normally distributed random numbers independent of a simulation program or within such a program.

Kovach states Ref. 6 :

"(Random) numbers generated by the computer are sometimescalled pseudo-random because they are subject to the limitations of the computer. In a list of truly random numbers, for example, one would expect to find numbers containing more digits than can be obtained in a computer."

Random numbers produced by the TI 59 ML-15 program are generated by a mathematical formula. Given an initial seed number by the user, this

program will always produce the same list of pseudo-random numbers. Thus if repeatedly initialized with the same seed number the forth-coming random numbers would be known and randomness would not exist. That is, every future random number could be predicted. Hence, the randomness of the numbers produced by the ML-15 program are as dependent upon the user as the mathematical formula of the program itself. It is therefore incumbent upon the routine user of the ML-15 program to vary the seed number used within denoted limits to insure genuine pseudo-random numbers.

The TI 59 ML-15 random number generator program is listed in Table 2-1. User instructions for the ML-15 program Ref. 11 are listed in Table 2-2. Data register contents are listed in Table 2-3.

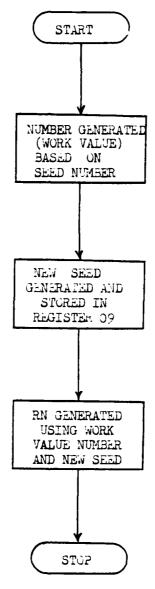
While the program does provide the option of generating uniform numbers for ranges other than 0-1 and also provides statistical data for the random numbers generated, only the generation of the uniform, range 0-1, and the normal random numbers will be discussed further.

### 1. Uniform Random Number Generator

A flowchart of the uniform random number generator, range 0-1, is displayed in figure 2-1. Program steps 000 through 054 contain the following mathematical formula, called the linear congruential method Ref. 11, for the generation of these numbers. (Throughout this thesis an asterisk is used to indicate multiplication.)

((24298 \* SEED + 99991) : 199017 STO 07)

A work value is the result of the above operation. This result remains in the display register. The value 199017 is stored in data register 07, an ML-15 work register.



TI 59 Uniform Random Number Generator FIGURE 2-1

Calculation continues.

(INV INT \* RCL 07) STO 09

The integer portion of the number resulting from the previous operation is discarded, then the remaining fractional portion is multiplied by 199017 which was stored in data register 07. This product then is stored in data register 09 and becomes the seed for the next random number calculation. Calculation continues.

((RCL 09 ÷ RCL 07) \* 5 INV 2nd log)

Now the new seed is divided by the number 199017 which was stored in data register 07 during the first operation. This quotient is then multiplied by the common antilogarithm of 5 to complete the step. Calculation continues.

(INT ÷ 5 INV log)

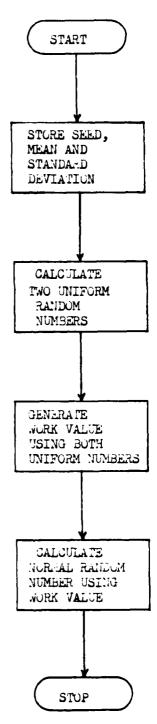
The fractional portion of the previous numerical operation is discarded and the result divided by the common antilogarithm of 5. This quotient is then displayed as the uniform random number, range 0-1.

### 2. Normal Random Number Generator

A flowchart of the normal random number generator is displayed in figure 2-2. Program steps 069 through 135 contain the following mathematical formula, called the direct method Ref. 1] for the generation of these numbers.

(seed STO 09)
(mean STO 10)
(standard deviation STO 11)

Following program initialization, three data values are entered and stored in data registers 09, 10, 11. The seed number, the desired normal distribution mean (mu) and the desired normal standard deviation



TI 59 Normal Random Number Generator FIGURE 2-2

(sigma) are stored in these registers as listed respectively. The seed value is limited as noted in the TI user instructions, table 2-2.

(SBR DMS STO 08 SBR DMS)

Initially the program calls the previously discussed uniform random number generator to produce such a number and then stores it in data register 08. The uniform generator is called again to produce another uniform random number which remains in the display register for manipulation and is denoted RN. Calculation continues.

((RN \* 2 \* 17 ) COS) \* ((RCL 08 LnX) \* (-2)

The uniform random number in the display is next multiplied by two pi.

The cosine of this product is then calculated. The resulting value is multiplied by the product of the natural logarithm of the first uniform random number (generated early and stored in data register 09) multiplied by negative two. This product remains in the display register for manipulation. Calculation continues.

( \* RCL 11) + RCL 10

The squareroot of the previous operation end value is multiplied by the desired standard deviation. Finally, this product is added to the desired mean, resulting in the generated normal random number. Seed manipulation for the generation of successive normal random numbers is completed during the SBR D.MS portion of the normal generation program.

### 3. SBR 2nd D.MS

The TI 59 ML 15 program does compile statistical data to allow computation of the mean and standard deviation of the pseudo-random numbers generated when using the normal distribution routine and the

uniform distribution routine over ranges other than 0-1. However, these data are not compiled when SBR 2nd D.MS sequence is executed to produce uniformly distributed numbers over the 0-1 range. Data registers one through eleven are used by the ML-15 program to compile and compute these statistics. Hence, if this program is called to produce normal random numbers within a larger program, such as a simulation, the use of these eleven data registers must be forgone. Yet, if the ML-15 program is called only to produce uniform random numbers over the range 0-1, only data registers seven and nine are used by ML-15, freeing nine registers for other use. This aspect of the TI 59 ML-15 program must be carefully considered when utilizing it is as a subroutine within another program.

#### C. COMBAT MODELS

Today there are considered to be three types of combat models in use; war games, pure simulations and analytical models. War games are models and games  $\begin{bmatrix} Ref. & 2 \end{bmatrix}$ :

" . . . in which individuals simulating decision makers in real life use their judgement to perform the decision functions in the model."

A war game may include automation to assist in the processing of data and the generation of random numbers to determine the outcome of certain chance events. A war game may also be a player-assisted simulation where players provide input to a computer model based on output (readouts) during a simulated battle. In comparison with the other models, war games appear to be more realistic, involve greater player interaction, are less automated, require much more time to run, more resources and involve a smaller degree of abstraction.

Simulation combat models are models Ref. 2 :

"... which run completely without human intervention. In this type of model events in the different combat processes are based on predetermined rules which are programmed into the automated evaluation procedure."

Combat models of this type generally contain a significant number of the important stochastic elements of combat in an attempt to simulate real battle. These models use probability distributions for the many chance input variables and produce probability distributions as results.

They utilize the Monte Carlo technique, repeatedly sampling all input distributions in the programmed sequence to produce a distribution of probable battle results for each set of input data.

Analytical models are models [Ref. 2]:

"... comprised of sets of mathematical equations as models of all the basic events and activities in the process being described and an overall assumed mathematical structure of the process into which the event or activity descriptions are integrated. "

While analytical models are the most time efficient they are also the most abstract and difficult to understand. As with the pure simulation, there is no human intervention when an analytical model is used.

All three models represent abstractions of the real world. The models themselves can be observed more conveniently than the real world and theories about the real world can be developed by studying the results of these models. Subsequently, these theories can be used to make predictions about real world events.

Each model type has strengths and limitations, some noted above and others listed in table 2-4  $\begin{bmatrix} \text{Ref. 2} \end{bmatrix}$ .

### 1. Pure Combat Simulations

Pure combat simulations are normally viewed as production tools, using Monte Carlo techniques to obtain results enabling the prediction of future system performance. But because the real world is so complex and interactive, attempts to model every detail of a large system in a pure simulation and to include every element that may influence the system can result in simulations so large and so complex that they are understood only by their developers and not by other users or decision makers. To avoid this complex dilemma, analytical models can be used to represent elements of the system being modeled instead of simulating the element itself and its inherent stochastic processes with every trial. This technique has been followed to some degree in the pure simulation model presented in Chapter III where the calculation of detection probability is an analytical model with results based on target range.

It should be noted that few, if any, simulation models ever completely include all those elements and events that affect the system(s) under study. Reference 2 points out that:

". . . a model is always incomplete, with only those aspects represented that we believe we know well enough to model and that we consider important in the issues to be examined with the model. Obviously, models tend to be as simple and concise as our knowledge of the activity warrants."

This is reflected in the model presented in Chapter III. While all the factors affecting system performance have not been directly simulated they are included either as analytical models or as given in the scenario.

Finally, a point to be stressed is that simulations need not be large to be useful, nor require the use of a large electronic digital computer to be credible. Using large computers for large problems and small computers for small problems is a rule of thumb that may overstate the case but certainly does not exaggerate it. Use of the TI 59 as a computer to tackle the problem set forth in Chapter III is an example of matching the problem to the computing power required. It is also an excellent example of the computing power of the TI 59.

```
000
       76 LBL
001
       88 DMS
002
       53
53
             ſ,
003
             €
004
       02
            24200
005
       04
006
       02
       09
08
007
008
009
       65
            \times
010
       43
           RCL
011
       09
            09
012
       85
             +
013
       09
             9
            900
       09
014
015
016
       09
       09
017
       01
018
019
       54
55
020
       01
            1
            99
021
       09
022
       09
023
       00
            Q
024
            1
       01
025
       07
       42 STO
026
027
      07
            07
028
       54
029
030
      53
53
031
      53
032
      22 INV
033
      59 INT
034
      65
           \times
035
      43 RCL
036
      07
            OF
037
      54
038
      42 STO
039
      09
            09
040
      55
```

TI 59 ML-15

Program

TABLE 2-1.1

```
43 RCL
07 07
041
042
043
        65
               [\times]
        05 5
22 INV
044
045
046
        28 LOG
047
        54
        59 INT
048
049
        55
              ÷
        05 5
22 INV
              5
050
051
052
        28 LOG
053
        54
        92 RTN
76 LBL
13 C
71 SBR
054
055
056
057
058
059
        88 DMS
        53
        24 CE
060
        65
061
              ×
062
        53
              (
        43 RCL
11 11
063
        11 11
75 -
43 RCL
10 10
064
065
066
067
068
        54
               )
069
070
071
072
073
        76 LBL
37 P/R
        35
        43 RCL
        10
              10
074
        54
              )
075
076
        42 STO
        07
              07
        78 I+
43 RCL
077
078
079
        07
              -07
080
        92 RTM
```

TABLE 2-1.2

```
081
                        76 LSL
18 C'
        082
083
084
                       70 RAI
71 SBR
88 DMS
        085
                              570
03
588
DMS
        086
                       42
        087
                    07833452
552452
        088
       089
 090
0912
0992
0995
0995
0995
0995
1002
1005
1007
1102
1102
1103
1103
1112
1113
                              .
CE
                                 <u>-</u>
                  50504446
50504446
                               \mathbb{K}
                  65
                43 RCL:: GTD RCL:: M
11567
1118
1118
1118
1118
1118
                36 PGM
                01
                          0.
               71 SER
25 CLR
92 RTH
 TABLE 2-1.3
```

```
121
122
123
124
125
126
127
128
129
130
131
132
133
134
135
                   76 LBL
15 E
                 15 E
42 STD
09 09
92 RTH
76 LBL
                  11
                           Ĥ
                 42 STO
               10 10
92 RTN
76 LBL
12 B
42 STD
11 11
               11 11
92 RTH
               ΟŪ
                           0
137
               00
                           0
138
139
140
               00
                          O
               00
                          0
              00
                          0
```

TABLE 2-1.4

TI 59 PROGRAM ML-15

# USER INSTRUCTIONS

# (MASTER LIBRARY MODULE)

STEP	PROCEDURE	ENTER	PRESS	DISPLAY
1	SELECT PROGRAM		2d PGM 15	
2	INITIALIZE		2đ E'	o l
3	ENTER RANDOM NUMBER SEED	SEED	E	SEED
	(0 <b>≤</b> SEED <b>≤</b> 199017)			
	FOR NORMAL DISTRIBUTION			
4	ENTER DESIRED MEAN	₮	A	
5	ENTER DESIRED STANDARD			
	DEVIATION	0	В	
6	GENERATE RANDOM NUMBER			
	(REPEAT AS NEEDED)		2d C'	RANDOM NUMBER
	FOR UNIFORM DISTRIBUTION			
	RANGE (0, 1)			
7	GENERATE RANDOM NUMBER			
	(REPEAT AS NEEDED)		SBR 2d D.MS	RANDOM NUMBER

### TI 59 PROGRAM ML-15

### DATA REGISTER CONTENTS

# REGISTERS:

$$R_{01}$$
  $\Sigma y$ 

$$R_{04}$$
  $\sum X^2$ 

$$R_{06}$$
  $\Sigma \times y$ 

TABLE 2-3

#### War Games

Intelligent play of decision maker.

Intelligent use of intelligence.

Can plan engagement and moves in advance.

Adapts maneuver to situation.

Can play many tactical situations (employment, penetration, etc.).

Insight is gained by understanding the particular rationale used in the decision process in single situations analyzed.

Controller determines existence of engagement and pace of play.

Very slow and costly in resources.

Very few situations can be examined.

Greatest visibility for the user.

Can include direct involvement by user.

## Simulations

Stylized decision routines, usually fixed throughout game.

Very limited use of intelligence.

Very limited planning horizon.

Very limited adapted maneuver routines.

Usually stylized maneuver, limited change in formations.

Insight is gained by repeating the analysis in many situations using different values for key parameters.

Predetermined scenarios and engagement rules -- combat very intense.

Faster to run after completely developed.

Many situations can be played and the sensitivity of key variables can be tested.

Reference 1, FM 44-90, Headquarters Department of the Army, 1977

TABLE 2-4

### III. COMBAT SIMULATION USING TI 59

This is a probabilistic duel simulation model, a pure simulation of a combat air battle, designed to reflect the characteristics of the Improved HAWK air defense artillery system (battery) in the manual mode under attack by a single cruise missile of sustained altitude, speed and direction.

The program scenario and engagement rules are predetermined with no user input once the simulation run has begun. Insight may be gained and the sensitivity of key variables tested dependent upon the use of different values entered by the user for these variables during program initialization. (Variables listed under E below.)

The model provides IHAWK system status, target engagement events and battle results as they are determined/occur. Only two battle results are possible: a "KILL" of the cruise missile or a unit "PENETRATION" by the cruise missile.

Given the operational ready rates of the major subsystems of the IHAWK system, the  $P_{\rm SSk}$  (probability of single shot kill) and the mean and standard deviation of lock-on-to-target times, the model samples from the uniform and normal distribution to determine system status, IHAWK missile kill or no kill and lock-on times. Target detection is modeled as a function of target range and is represented as a linear relationship in the simulation.

This simulation was developed to exhibit the computing power of the TI 59 and to determine if one parameter under the control of the IHAWK

battery commander could significantly affect air battle results. This parameter was the tracking radar "lock-on-to-target" time which is a function of operator training given (1) a manual mode operation, and (2) perfect equipment. The sensitivity of battle results to varying lock-on times is listed under F below.

### A. IHAWK SYSTEM

To be effective, an air defense system must be able to detect, identify, engage and destroy an airborne target. The IHAWK system can engage and destroy a full spectrum of threat aircraft and missiles operating throughout a wide range of tactical speeds and altitudes. It can engage a multiple target threat as well as single targets. The system is effective from ground level up to altitudes of about 48000 feet and out to ranges of about 40 kilometers. The system can operate at night, under all conditions of weather and reduced visibility. It can function effectively in an ECM (electronic countermeasures) environment and is mobile using organic unit vehicles or helicopters [Ref. 1]. However, some adverse weather and heavy ECM may diminish some system capabilities.

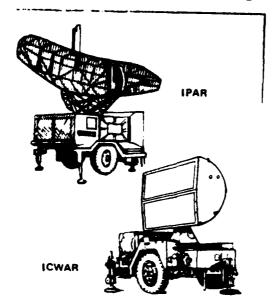
This simulation does not model: (1) weather

- (1) Weather
- (2) detection ECM
- (3) visibility
- (4) system mobility

#### 1. Detection

Target detection is accomplished by either the improved pulse acquisition radar (IPAR) or the improved continuous wave acquisition radar (ICWAR), or both. The IPAR can detect low to medium altitude targets out to ranges in excess of 100 kilometers while the ICWAR can detect targets at very low altitudes with ranges in excess of 60





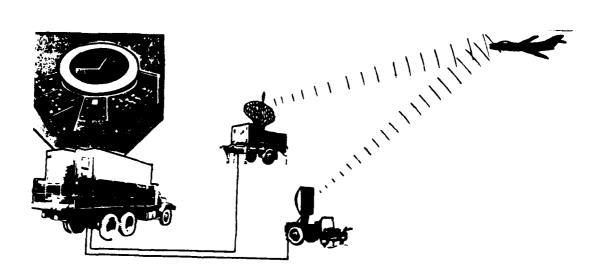


Figure 3-1

kilometers. Operating on the doppler principle, the ICWAR sees only very low moving objects and not stationary objects on the ground.

Detection may be reduced if terrain features such as hills, trees and buildings mask the radar's view of the approaching target. Even with completely level terrain, the earth's curvature causes a reduction in the detection and tracking ranges of the system against very low-altitude targets. Also, evasive maneuvers by threat targets may reduce the detection and tracking ranges and increase system response time, thereby reducing the effective or intercept range. This simulation does not

#### model:

- (1) terrain features
- (2) curvature of the earth
- (3) evasive action by targets
- (4) pulse detection or continuous wave detection per se

#### This model assumes:

- (1) clear weather
- (2) no detection electronic countermeasures
- (3) line of sight (LOS) exists between radar and target
- (4) flat desert terrain
- (5) nonmaneuvering target
- (6) only one attacking target exists
- (7) target is a cruise missile of constant speed and constant altitude
- (8) detection is a function of target range

The probability of detection is modeled during each sweep of the radar as a linear function of target range from the battery as follows: For the IPAR the  $P_{DET} = (-.25 \div 65)$  \* Target Range + 1.0 For the ICWAR the  $P_{DET} = (-.5 \div 65)$  \* Target Range + 1.0 The probability of detection is calculated every three seconds of simulated time. This is based on the radar rotation rate of 20 revolutions per minute. That is, every three seconds each radar takes a 360 degree glimpse of the horizon. The radars are slaved to

each other and rotate in synchronization. Additionally, the IPAR is modeled to detect only targets from 5000 to 40000 feet in altitude while the ICWAR detects targets from 1 to 8000 feet in altitude. Thus the battery's very low and low to medium detection capability is dependent upon the operational status of these radars as noted. Targets above 40,000 feet cannot be detected in this simulation. The operational ready rates of these two radars has been arbitrarily set at .65 (ICWAR) and .95 (IPAR).

# 2. Identification

Identification of any potential target is accomplished by means of the identification, friend or foe (IFF), equipment of the IHAWK system and/or other established hostile criteria. If the target cannot be positively identified in this simulation because of a non-operational IFF, the target speed and altitude is checked to determine target status (foe or not foe). That is, if the IFF is nonoperational and if the target is below 5000 feet altitude and greater than 550 KMPH in speed, it is identified as a foe; otherwise, it is not a foe.

This model assumes: (1) once identified as a friend, always a friend, (2) once identified as a foe, always a foe.

The operational ready rate of the IFF has been arbitrarily set at 95 percent. This model does play IFF accuracy to the degree that an operational IFF will be in error two percent of the time. That is, a foe will be shown to be a friend two percent of the time. This model assumes operational IFF accuracy to be 98 percent.

**1** Identify

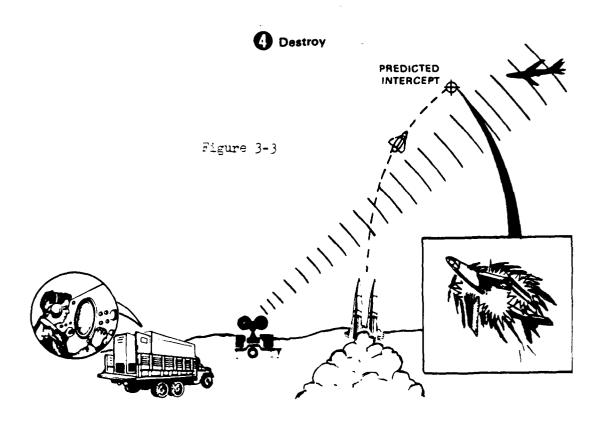
Figure 3-2

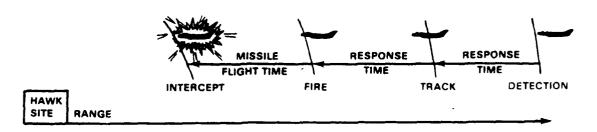
— CORRECT RESPONSE (FRIEND) — NO RESPONSE OR INCORRECT RESPONSE (FOE)

3 Engage

# 3. Engagement/Destruction

The IHAWK battery has two firing sections, each of which contains a target tracking radar which is called an improved high powered illuminating radar (IHIPIR), and three launchers with three missiles each. If a potential target is determined to be a foe, it is assigned to one or both of these firing sections. The tracking radar of these sections, under the control of a fire control operator (enlisted personnel), attempts to lock-on to the approaching hostile target. The operator directs the automatic box search of the radar in the azimuth and expected elevation of the target in attempting this target lock. The operator's ability to achieve a target lock is a function of his training given the condition mentioned above. The time that elapses in attempting this target lock is extremely important. Target engagement cannot continue without target lock and the longer it takes to achieve target lock the closer the target moves toward the battery, reducing the intercept range. Tracking radar lock-on times are assumed to be normally distributed. After target lock has been achieved and the target is in range, one or two missiles are fired on order from the unit tactical control officer in a battery control van. Engagement is continued until the target is destroyed or until engagement is no longer possible. This simulation models each firing section as an entity. After a target has been declared a foe and assigned to one or both firing sections, this model simulates the target lock-on time by utilizing the TI 59 normal random number generator based on a normal mu and sigma input by the user during initialization.





The range at intercept is determined by the range at which detection and tracking (lock-on by the HIPIR) occur and on system response time.

In this model, targets are engaged that are:

- (1) declared to be foe
- (2) less than 40 KM from the battery
- (3) greater than 8 KM from the battery

## This model assumes:

- (1) two independent firing sections
- (2) salvo fire occurs if both sections are operational and shoot-look-shoot if only one section is operational
- (3) firing continues until kill or penetration
- (4) penetration means that the target is 8 KM or less from the battery
- (5) lock-on-to-target time is a function of operator training and is normally distributed
- (6)  $P_{ssk} = .75$  (arbitrarily set)

The operational ready rate of each firing section has been arbitrarily set at 75 percent.

## 4. Target

The target for this model is assumed to be a hostile cruise missile that flies straight in toward the battery at a constant speed and altitude as established by the user during initialization. The initial range of the target is also a user input. The lethality of the missile warhead is assumed to be such that any successful penetration by the missile to within 8 KM or less of the battery before destruction is considered a total penetration of the battery defended area. Therefore, the target must be destroyed before 8 KM to score a kill. Additionally, a target will not be engaged after detection until it is less than 40 KM from the battery and no further missiles will be fired at the target once it is within 8 KM of the battery. The target speed has a lower bound of 100 KMPH but no upper bound. Only targets between 1 and 40000 feet in altitude can be detected and are thus the altitude bounds. Finally, all targets are hostile and will be engaged

unless erroneously identified as friendly or not foe, resulting in a free penetration.

# 5. Time

This simulation is a time step model, updating all battery events and functions every three seconds of simulated time. This three-second interval stems from the rotation rate of the detection radars, 20 revolutions per minute or one complete rotation (scan of the horizon) every three seconds.

## B. MACRO FLOW CHART

The enclosed macro flow chart, figure 3-4, depicts the general flow of the simulation logic from start to either penetration or kill.

First the model determines if a detection capability exists. This could be one or both of the detection radars. Using the internal random number generator of the TI 59 for a 0-1 uniform distribution, two random numbers are drawn and compared with the detection radar operational ready rates. If the random number is less than the rate, the radar is operational; otherwise, it is nonoperational. If no detection capability exists the simulation is terminated by a penetration of the defended area by the target.

Detection of the target is based partly on the formulas set forth above and results of the 0-1 range uniform random number generator. The probability of detection is based on the range of the approaching target and is recalculated every three seconds. The probability of detection for each radar is compared with a generated random number between 0 and 1. If the random number is less than the probability

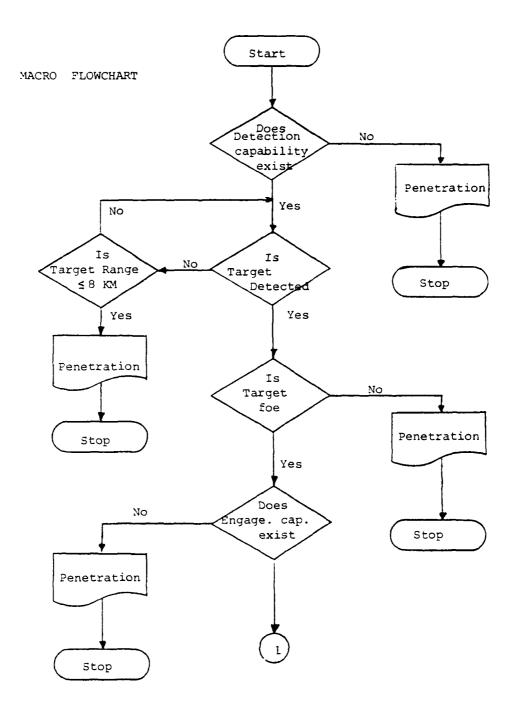


Figure 3-4.1

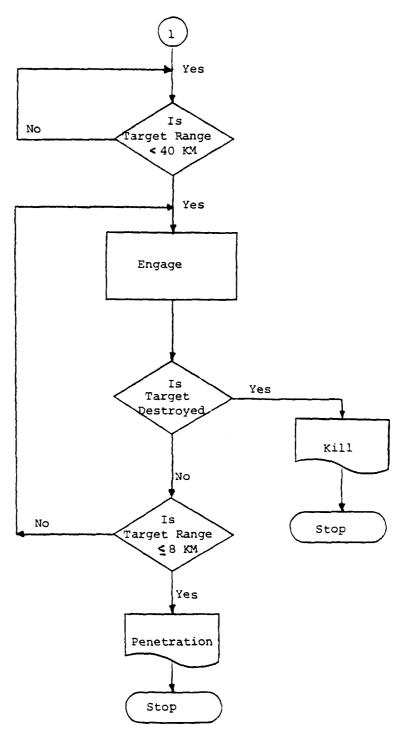


Figure 3-4.2

the target is detected; otherwise, it is not. As the target moves closer to the unit, the probability of detection increases linearly. However, detection is not based on range alone. The target must be within the detection altitude carability of the operational system. For instance, if the battery's detection capability rests solely on the IPAR because of a nonoperational ICWAR and if the approaching target is at an altitude of less than 5000 feet, detection will never occur and a penetration will result.

Identification of the target is determined by either the IFF or a combination speed and altitude envelope if the IFF is nonoperational. Operational status of the IFF is determined by comparing, again, a generated random number from a 0-1 range uniform distribution against the operational ready rate of the IFF. If the random number is less than the ready rate, the IFF is operational; otherwise, it is nonoperational. If the IFF is nonoperational and if the unit has a tracking capability, the target speed and altitude can be checked against an established hostile criteria. If the target is found to be below 5000 feet in elevation and above 550 KMPH in speed, it is designated a foe; otherwise, it is considered to not be a foe. Only targets positively identified as foes are engaged.

IFF positive identification of the hostile cruise missile as a foe is determined by comparing a random number generated from a 0-1 range uniform distribution against the IFF accuracy rate of 98 percent. If the random number is less than the accuracy rate, the cruise missile is correctly identified as a foe; otherwise, it is erroneously classified as a friend resulting in a penetration of the defended area.

The battery's engagement capability lies with its two firing sections, each tracking and firing on approaching hostile targets. Again, two random numbers drawn from the 0-1 uniform distribution are compared to the operational ready rates of the firing sections to determine the status as in the previous subsystems examples. If an engagement capability is determined to exist, the process continues on to direct missile firings at the target following target lock by the tracking radar(s). As mentioned earlier, this lock-on time is a function of operator training in the manual mode and is normally distributed. For highly trained operators the mean is assumed to be ten seconds with a standard deviation of five seconds. The lock-on time for each section is determined by two random numbers generated by the TI 59 random number generator from a normal distribution with mean and standard deviation determined by the user during program initialization. (Any random number less than zero is discarded and another generated to avoid negative times.) The length of the lock-on period directly affects the resultant target intercept range. If the lock-on time is sufficiently long the missile firing is delayed and the probability of a penetration is likely. (The determination of air battle results to varying lock-on times provided the basis for the development of this simulation, though other variables of the model can easily be tested for outcome sensitivity.) Again, targets are not engaged until less than 40 KM from the battery and no missiles are fired after the target is 8 KM or less from the battery.

Missile effectiveness after firing is determined when the IHAWK missile range equals or exceeds the cruise missile range from the

battery. A random number from a 0-1 range uniform distribution is generated for each missile fired and checked against the  $P_{\rm SSk}$ . Random numbers less than the  $P_{\rm SSk}$  result in kills while all others result in no kills. Engagement of the target continues until a kill or penetration is registered.

## C. MICRO FLOWCHART

The micro flowchart in appendix A depicts the detailed flow of processing throughout the simulation from start to kill or penetration.

D. SUBROUTINES, LABELS, FLAGS, DATA REGISTERS AND PROGRAM MEMORY STEPS

# 1. Subroutines and Labels

This simulation uses 49 of the 72 labels available for programming on the TI 59. Of these 49, 14 are subroutines. The remaining labels are used to identify sections of the program and to direct action to these sections during simulation runs. A complete listing of all labels is displayed in table 3-1 with the subroutines marked by an asterisk. Comments on selected labels and a printout of the entire program is enclosed in appendix A.

## 2. Flags

Nine of ten available flags are used. As the IHAWK equipment and target friend/foe status is determined, this model uses TI 59 flags to maintain a record of the system and target status. These flags subsequently direct the flow of processing and determine actions to be taken within the simulation engagement.

Flag 1 set means the target has been detected. Flag 2 set means the target is a friend. Flag 3 set means the ICWAR and the IPAR

are operational. Flag 4 set means only the ICWAR is operational. Flag 5 set means only the IPAR is operational. Flag 6 set means the IFF is operational. Flag 7 set means that alfa firing section is operational and bravo firing section is nonoperational. Flag 8 set means that bravo firing section is operational and alfa firing section is nonoperational. Flag 0 set means that both firing sections are operational.

## 3. Data Registers

The TI 59 memory storage area is initially partitioned to provide 60 data storage registers and 480 program storage locations. However, the user can repartition the memory storage area to suit his particular programming needs. The IHAWK simulation requires exactly 800 program memory locations and 20 data storage registers. Within the TI 59 there are a total of 120 registers to be used for data storage and program locations. While each register can store only one datum point, each can store eight program instructions or steps. Thus 3 \* 60 = 480 program locations which are initially available as mentioned above. Repartitioning the core 120 registers is done in increments of ten. Hence, to get the 800 program steps for the IHAWK simulation 100 core registers are needed. This leaves exactly the 20 needed for data storage.

To partition the storage area, the number of sets of 10 data registers needed is entered and 2nd OP 17 pressed. Thus for the IHAWK simulation, twenty data registers are available after the initial repartitioning by pressing 2 2nd OP 17. The registers and their contents are listed on the following page.

- R<sub>00</sub> Target range. Entered by user,
- $R_{01}$   $R_{01}$  through  $R_{08}$  are used by the TI 59 random number generator program.

 $R_{02}$ 

R<sub>03</sub>

R<sub>04</sub>

R<sub>05</sub>

R<sub>06</sub>

R<sub>0.7</sub>

R<sub>08</sub>

- $R_{09}$  SEED for random number generator. Entered by user.
- R<sub>10</sub> Mean lock-on-to-target time. Entered by user.
- $R_{11}$  Standard deviation of lock-on-to-target time. Entered by user.
- $R_{12}$  IHAWK missile range from battery. Initially zero.
- $R_{13}$  IHAWK missile range from battery. Initially zero.
- R<sub>14</sub> Probability of detection work register.
- R<sub>15</sub> Target speed. Entered by User.
- R<sub>16</sub> Target altitude. Entered by User.
- $R_{17}$  Target range work register. Not entered by user.
- $R_{18}$  Simulation trials or runs to be completed. Entered by user.
- ${\bf R}_{19}$  Simulated time in seconds for each trial. Initially zero for each trial.

# 4. Program Memory Steps

There are 800 program steps available. All 800 program memory steps are used in this program.

## E. USER INSTRUCTIONS

The enclosed user instructions, table 3-2, provide the necessary steps to initiate a sequence of simulation runs. The enclosed printout results, table 3-3, indicate the 22 possible print statements that may occur during the simulation. A sample of data input and simulation run results are displayed in tables 3-4 and 3-5.

Two steps of the user instructions warrant further comment.

## 1. Step 2 Clear Data Registers.

Instead of clearing all data registers the user may wish to clear selected registers when repeating simulation runs as in the case of sensitivity analysis work. In this instance the user may just clear registers  $R_{01}$ ,  $R_{12}$ ,  $R_{13}$ ,  $R_{17}$ ,  $R_{18}$ ,  $R_{19}$  and enter the desired values.  $R_{09}$  need not be reentered as the program automatically changes the seed after each random number is generated. If the user does clear all data registers with 2d CMs the user must then enter an entirely different seed in  $R_{09}$  within the bounds noted.

# 2. Step 9 Check Data Register Content

This step is a quick safeguard for the user to ensure that the simulation run is based on the correct parameter values. This step provides a complete listing of the 20 data registers with contents for review prior to the final user step.

# F. SENSITIVITY ANALYSIS RESULTS FOR LOCK-ON TIMES

Four hundred simulation runs were made with four lock-on mean values: 10, 20, 30 and 40 seconds. In each case the lock-on time standard deviation was five seconds. For each simulation run the

target was initially set at a range of 50 KM in  $R_{20}$ , target speed was 1500 KMPH and target altitude was 7000 feet. An initial random number seed was entered for run number one but no further user seeds were provided, thus leaving seed manipulation to the program.

The results listed below indicate that air battle results are indeed sensitive to target lock-on times.

LOCK-ON TIME		PENETRATION	KILL
mu	sigma		
10	5	11%	89%
20	5	14%	36 %
30	5	26%	743
40	5	44%	56₹

The results indicate a significant increase (12 percent) in defended area penetrations for a mu of 30 under the present scenario. This trend continues at an apparent exponential rate. With a mu of 40 seconds, defended area penetrations increase another 18 percent. Eased on these results it appears advisable to maintain such a state of operator training that the mean target lock-on times be twenty seconds or less with as little deviation among the operators as possible. Furthermore, it seems that for the extra training assumed to be required to reduce mean lock-on times from 20 to 10 seconds there appears to be only a small marginal reward in the reduction of defended area penetrations (3 percent).

## G. RECOMMENDATIONS

While the intent throughout the thesis is to exemplify the capabilities of the TI 59 as a viable, real world analytical tool, the results of the TI 59 simulation lend insight into an area that requires

further investigation, that being IHAWK target lock-on times. While only the lock-on times themselves were varied for this simulation, other important scenario parameters should be varied to acquire an improved understanding of how air battle results can be affected by lock-on times.

Future enhancements of these results would include a significant increase in simulation runs for a wide variety of scenario parameter settings. While this TI 59 model allows certain parameter variations during program initialization, other parameters such as acquisition radar altitude detection capabilities can be varied with only minor adjustments to the program.

Regardless of whether future simulation studies are conducted using this TI 59 model or a facsimile on another computer, the results above warrant further research in this area.

```
930
       39 505
 045
       30 TAN
       60 DEG
 060
 067
       69 DP
 099
       17 8*
 135
       98 ADW
158
170
       90 LST
       42 STO
       18 0
 180
 203
       14
           D
       16 A*
 208
       43 RCL
 222
 231
235
       33 X2
       15
           Ε
       52 EE
 251
 259
       10 E'
 278
       19 D'
 297
       67
          Εũ
       88 DMS
 318
       34 1%
,334
338
       23 LNM
 354
       24 CE
 359
378
393
       22 INV
       32 X4T
       25 CLR
 411
       28 LDG
 455
       38 SIN
       37 P/R
*491
       49 PRD
 502
 510
       11
            A
 535
       12
            E
 560
       13
           i)
*585
       50 IN I
           5
*601
       89
*610
       79
       59 INT
*627
       48 E.K
#633
*639
       80 GRD
                         Table 3-1
*654
       70 RAD
 660
       68 NOF
 667
677
       97 DSC
58 FIX
*685
       57 ENG
       29 CF
*708
*722
       96 WET
*731
       78 I+
*745
*760
       35 1/3
       45 98
 766
       44 SUM
```

USER INSTRUCTIONS				
STEP	PROCEDURE	ENTER	PRESS	DISPLAY
1	REPARTITION	2	2d OP 17	799.19
	800 PROGRAM MEMORY LOCATIONS 20 DATA MEMORY REGISTERS			
2	Enter magnetic program cards, sides 1 through 4			
3	CLEAR DATA REGISTERS		2nd CMs	(NO CHANGE)
4	RESET ALL FLAGS AND CLEAR ALL SUBROUTINE RETURN REGISTERS		RST	(NO CHANGE)
5	ENTER IHAWK SYSTEM DATA			
	TRACKING RADAR "LOCK-ON" TIME	u v	STO 10 STO 11	u T
6	ENTER CRUISE MISSILE DATA	RANGE (KM) 10 < KM < 100	GTO 777 LRN LRN	
		RANGE (KM)	STO 00	RANGE
		10 < KM < 100 SPEED ALTITUDE (FT)	STO 15 STO 16	SPEED ALTITUDE
7	ENTER SEED FOR RANDOM NUMBER GENERATOR (0 ≤ S ≤ 199017)	SEED	STO 09	SEED
8	ENTER DESIRED NUMBER OF SIMULATION RUNS	#	STO 18	#

Table 3-2.1

USER INSTRUCTIONS				
STEP	PROCEDURE	ENTER	PRESS	DISPLAY
9	CHECK DATA REGISTER CONTENT	0	RST INV 2d LIST	0
10	START SIMULATION RUN		R/S	(SEE RESULTS POSSIBLE)*
	* PC-100 C PRINTER REQUI	RED		

Table 3-2.2

# RESULT PRINTOUTS

NUMBER PRINTED	MEANING
1	CRUISE MISSILE HAS BEEN DETECTED AT (RANGE GIVEN IN KMs FROM UNIT)
3	LOW ALTITUDE DETECTION RADAR (ICWAR) AND MEDIUM ALTITUDE DETECTION RADAR (IPAR) ARE BOTH OPERATIONAL
4	ONLY ICWAR IS OPERATIONAL
5	ONLY IPAR IS OPERATIONAL
6	IDENTIFICATION FRIEND-OR-FOE (IFF) IS OPERATIONAL
7	ALFA FIRING SECTION IS OPERATIONAL, BRAVO FIRING SECTION IS NONOPERATIONAL
8	BRAVO FIRING SECTION IS OPERATIONAL, ALFA FIRING SECTION IS NONOPERATIONAL
9	BOTH FIRING SECTIONS ARE OPERATIONAL
10	CRUISE MISSILE IS IDENTIFIED AS A FOE
11	BRAVO FIRING SECTION IS FIRING ONE MISSILE AT A TARGET < 40 KM FROM THE BATTERY, BUT GREATER THAN 8 KM
12	ALFA FIRING SECTION IS FIRING ONE MISSILE AT A TARGET < 40 KM FROM THE BATTERY, BUT GREATER THAN 8 KM
14	CRUISE MISSILE IS ERRONEOUSLY IDENTIFIED AS A FRIEND BY IFF
15	CRUISE MISSILE IDENTIFIED AS NOT FOE BY SPEED AND ALTITUDE CRITERIA, IFF IS NONOPERATION
17	ALFA FIRING SECTION IS OPERATIONAL
18	ALFA FIRING SECTION IS NONOPERATIONAL
23	BATTERY IS NONOPERATIONAL, NO DETECTION CAPABILITY
24	BATTERY IS NONOPERATIONAL, NO FIRING CAPABILITY
25	ALFA SECTION MISSILE "NO KILL" FOLLOWED BY RANGE (KM) OF APPROACHING TARGET

Table 3-3.1

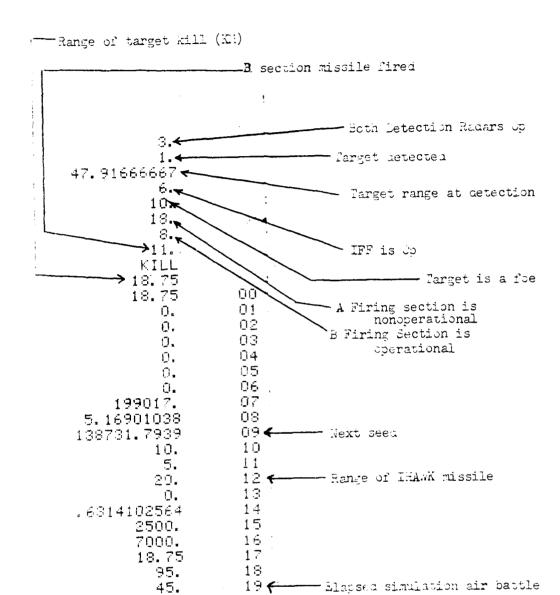
# RESULT PRINTOUTS

NUMBER PRINTED	MEANING
26	BRAVO SECTION MISSILE "NO KILL" FOLLOWED BY RANGE (KM) OF APPROACHING TARGET
66	IFF IS NONOPERATIONAL
	TARGET "KILLS" ARE SPELLED OUT, I.E. "KILL", FOLLOWED BY THE RANGE FROM THE UNIT AT WHICH THE TARGET WAS DESTROYED
	"PENETRATION" IS PRINTED WHEN A CRUISE MISSILE APPROACHED WITHIN 8 KMs OF THE BATTERY. IN THIS INSTANCE THE UNIT IS CONSIDERED PENETRATED AND DESTROYED

```
50.
                      □□ ← Initial Parget Range
                      01
           0.
                      02
03
04
           0.
           0.
            0.
                      05
06
07
            O.
            0,
            Į,
                       08
            0.
                       09 ←
111111.1111
                                  - kandom number seed
                       10 4
           30.
                                        - Mean lock-on time
            5.
                       11
            0.
                       12
            0.
                       13
                                               • Standard
                       14
            Ū.
                                                 aeviation time
        2500.
7000.
                       15 ◆
                                  -Target
                       16
                                  Speed (Kinks)
                       17
            ŋ.
                                          Target altitude
         100.
                       18
                                                (feet)
                       19
            Ũ.
                                           Simulation run #
```

Farameter Value Inputs To Selected Data Registers

Papie 3-4



Printout During Simulation an: Data Angister Contents
Pable 3-5

time

# IV. DATA ANALYSIS

## A. PURPOSE

The purpose of this chapter is to demonstrate how the TI 59 may be used to analyze data. Rather than use assumed or contrived data, an actual experiment was conducted by the authors for illustrative purposes. Strict requirements for random sampling were not met in conducting the experiment but, again, the purpose of this thesis is to demonstrate the capabilities of the TI 59 rather than to make inferences or draw broad conclusions from the experimental data.

Before discussing methods for data analysis, the scope, design, and methodology of the experiment will be presented in sufficient detail to make the data analysis meaningful. Presentation of the experiment will be followed by a detailed discussion of a TI 59 program designed to compute measures of central tendency and spread for sample data. Chapter V discusses a TI 59 program which may be used to make statistical inferences using the same experimental data.

## B. FITNESS EXPERIMENT

# 1. Scope of the Experiment

The experiment was conducted to test the hypothesis that different physical conditioning programs result in different levels of physical fitness. Six different conditioning programs were evaluated using five tests. The scope of the experiment was limited to testing the strength and endurance of selected upper body muscles, together with overall cardiovascular fitness. A completely comprehensive fitness

evaluation would also include lower body strength and endurance as well as muscular flexibility and agility. Other factors such as diet, use of alcohol, tobacco and other drugs would also be requisite. This experiment was limited to the examination of thirty-six male subjects by the two authors to determine cardiovascular efficiency, bicep strength, bicep endurance, pectoral strength and pectoral endurance. Thirty of the subjects were military officers attending the Naval Postgraduate School. The other six subjects were weightlifters who trained at Bailey's Gym in Seaside, California. The subjects varied in age from nineteen to thirty-seven but were predominantly in their early thirties. While it is recognized that strict requirements for random sampling requisite for statistical analysis were not met in conducting the experiment, it should be pointed out that there is every reason to believe that the subjects examined were representative of the population from which students are continually drawn for the institution. Strict inference to any specified population will not be made, but as mentioned earlier the purpose of this discussion is to illustrate the use of programs developed for the TI 59, not to make inferences from the data gathered in this particular experiment.

Since the terms, strength, endurance, and cardiovascular efficiency are subject to a myriad of interpretations, the definitions used for this analysis are presented before proceeding to discuss the test methodology. Muscular strength is defined as the ability to exert maximum force against an object, while muscular endurance relates to the ability to exert force which is not necessarily maximal over an extended period of time. Cardiovascular efficiency relates to how

Before analyzing the results a thorough explanation of the experimental design and methodology is provided.

## 2. Experimental Design

The subjects were divided into six categories (each consisting of six individuals) based on their exercise programs. The following six categories were used: Category I - Individuals who had participated in no exercise over the last six months; Category II - Individuals who ran more than thirty miles per week and who did so for at least the last six months; Category III - Individuals whose exercise consisted solely of lifting weights, whether for power or building physique, and who lifted at least twice a week; Category IV - Individuals who lifted weights at least twice a week, who ran twenty or more miles per week and who did both the lifting and running for at least the last six months; Category V - Individuals who lifted weights at least twice a week, who ran between ten and nineteen miles per week, and who did the lifting and the running for at least the last six months; and Category VI - Individuals who did not run or lift weights but who participated in basketball, racquetball, bicycling, or judo on a regular basis.

Five tests were administered to each subject in each category.

Cardiovascular efficiency was measured using the Pipes Test for Cardiovascular Health, which consists of the following seven steps:

- 1. Have the subject lie quietly on a pad for ten minutes.
- 2. Take a pulse reading for the resting heart rate.

- Have the subject sit on a chair with his arms folded across his chest.
- 4. With his arms folded, have the subject stand up and sit down twice every five seconds for three minutes.
- 5. Take a reading for the heart rate immediately after sitting down at the conclusion of the three minute exercise.
- 6. Take readings at 30-second, 60-second, and 120-second intervals after the exercise to measure recovery heart rate.
- Using a table developed by Pipes and the five heart rate readings determine the cardiovascular health score.

This test, developed by an exercise physiologist, Ref. 9 is based on the premise that the heart rate describes an individual's fitness in three areas: how much oxygen he needs, how much blood his heart has to pump to meet the oxygen need, and how hard the heart works. Individuals with a low level of fitness do not extract oxygen efficiently from the blood so must pump more blood, resulting in a higher heart rate. In conducting the test, the same examiner took the pulse readings at the different intervals using the radial artery in the subject's wrist. The heart rate was monitored for ten seconds then multiplied by six to obtain the number of heart beats per minute.

The muscular strength test used for biceps was the maximum standing curl the individual could accomplish using a barbell. The proper technique was demonstrated to each subject by the examiner and lifts where the individual "cheated" by swinging the weight or arching his back were not counted. Bicep endurance was measured by the number of curl repetitions the subject performed with a 55 pound weight. These two tests were predicated on the generally accepted basis that curling

is the primary bicep exercise and that low repetition, high resistance exercises are best for developing endurance [Ref. 3]. Fifty-five pounds of weight were selected prior to the experiment as a low resistance weight well below each subject's strength capability and therefore in compliance with expert opinion that the force used for endurance testing should be considerably below the individual's static force capability [Ref. 7].

In a similar fashion, the bench press was used to test pectoral strength and endurance. Pectoral strength was measured by the maximum weight that the individual could bench press, while pectoral endurance was measured by the number of bench press repetitions he could perform.

Each subject was tested using an identical sequence of events. Initially each person was given an instruction sheet (table B-1 in Appendix B) which explained the purpose of the experiment and defined those attributes to be measured, i.e. muscular endurance, muscular strength, and cardiovascular health. The subject was then asked to complete a questionnaire (table B-2, Appendix B) concerning certain aspects of his medical history. Each man was instructed to stop the testing if he felt any significant level of pain. He was then asked to complete a form disclosing his name, age, weight, and height (table B-3, Appendix B). Next, one of the examiners questioned the subject concerning his exercise program over the last six months and made a subjective judgement as to which of the six categories he belonged in.

After this administrative procedure was completed, the actual testing was begun with the bench press test described above. (The

same examiner tested each of the thirty-six subjects in both the strength and endurance exercises in order to minimize any variance due to test administration.) The subject was shown how to do the bench press, allowed to practice once if desired, and then tested for the maximum number of repetitions he could perform with 100 pounds. The number of repetitions was recorded and the subject was allowed a three minute rest before being tested for his maximum bench press. The examiner estimated the amount that each subject could bench press and set up the weights accordingly. All adjusting of weight was done by the examiner so that the subject's lift capability was not degraded. The man was then asked to bench press the weight set up for him. If he was able to make the lift ten pounds were added and he was asked to try again. If he failed the second attempt he was given credit for five pounds less than he attempted. For example, if an initial attempt of 165 pounds was successful and a subsequent attempt of 175 pounds was missed, then the score was recorded as 170 pounds.

After another three minute rest the subject was tested on the number of times he could curl 55 pounds. This was followed by another three minute rest before testing for his maximum curl capability. Once again, the man's maximum lift was estimated by the examiner and all adjusting of the weight was done by the examiner.

Following the four lift tests, the Pipes Cardiovascular Health

Test [Ref. 9] was administered by the second examiner and the subject's testing was completed. Before examining the test results, a procedure for scoring the tests was requisite. Accordingly, the scoring procedure explained in the following discussion was decided upon.

# 3. Scoring Methodology

The heart rates recorded during the Pipes Cardiovascular Test were scored using table B-4 in Appendix B. Each subject's score for resting heart rate, heart rate immediately after the exercise and heart rate at the 30-second, 60-second, and 120-second intervals was aggregated to a total score ranging from zero to one hundred. This score was then used as the measure of cardiovascular fitness for comparative analysis.

In order to compare muscle strength among the subjects and among the categories, it was necessary to adjust each subject's lift for varying sizes and body structures. Accordingly, each man's maximum curl and maximum bench press were divided by his body weight, resulting in an adjusted score for each lift. These two adjusted scores were then added together to yield an upper body strength measure. For example, let S<sub>13</sub> be the strength measure for the third subject in Category I (where the first subscript indicates the category and the second indicates the subject within the category). The following formula may then be used to obtain the strength score for the third subject tested in Category I:

# S<sub>13</sub> = maximum bench + maximum curl body weight

As discussed earlier, muscle endurance was measured for the same two areas tested for strength - the biceps and the pectorals. The bicep endurance was measured by the maximum number of curl repetitions performed with 55 pounds, while the pectoral endurance was measured by the maximum number of bench presses accomplished with 100 pounds. As

in the case of strength, an adjustment was made for the subject's body weight. In the case of endurance, however, the amount of weight lifted (which was 55 pounds for the curl and 100 pounds for the bench press) was divided by the subject's body weight and then multiplied by the corresponding number of repetitions lifted. These two scores were then summed as the endurance index. For example, let  $E_{13}$  be the endurance score for the third subject tested in Category I. The following formula then obtains:

## 4. Test Results

Tables B-5 through B-10 in Appendix B reflect the results of the experiment for each of the six categories tested. For example, table B-5 depicts the age, weight, cardiovascular score, adjusted strength score and adjusted endurance score for each of the six subjects tested in Category I. Appropriate references are made at table B-5 for the development of the final cardiovascular, strength and endurance scores. The scoring methodology section of the chapter provides a detailed explanation of the rationale and methodology for deriving these scores.

## C. TI 59 FROGRAM FOR DATA ANALYSIS

Having developed the experimental design, the scoring methodology, and the test results it is now possible to analyze the data. Measures of

central tendency and spread will be used to illustrate an application of the TI 59 in analyzing sample data. The measures of central tendency used for this illustration are the mean,  $\overline{\mathbf{x}}$ , and the median. The measures of spread used are: the sample variance,  $\mathbf{s}^2$ ; the standard deviation,  $\mathbf{s}$ ; the mean absolute deviation, MAD: the mean squared deviation, MSD; the root mean squared deviation, RMSD; and the range. A TI 59 program will now be described in detail which computes these measures followed by an example applying the program to the results of the fitness experiment.

# 1. TI 59 Capabilities

The TI 59 has been hard-wired to calculate the sample mean and variance as well as MSD. As described in the TI 59 Personal Programming Manual [Ref. 12] if each datum is entered into the calculator followed by pressing the  $\Sigma$ + key, the calculator will sum each data entry,  $\kappa_i$ , into register one, sum the squares of  $\kappa_i$  into register two, store the number of data entries in register three, and calculate  $\overline{\kappa}$ ,  $s^2$ , and MSD. (By definition,  $s^2 = 1/n-1$   $\sum (\kappa_1 - \kappa)^2$  is the unbiased estimator for  $\sigma^2$  while MSD =  $(n-1)s^2/n$  is the maximum likelihood estimator.) Pressing the  $\overline{\kappa}$  key will yield the mean, INV  $\overline{\kappa}$  will display  $s^2$  and 2nd Op 11 will display MSD. If these are the only measures desired then utilization of the  $\Sigma$ + key is the most expedient method of obtaining them. The TI 59 statistics module has a program (Program 03) which computes these same measures as well as the middle value (MIDVAL). Additionally, Program 03 stores each data entry beginning with register 31. Program 03 also computes a number of other quantities not germane

to an analysis of the data gathered in the experiment discussed previously in this chapter. Since this results in a slightly longer run time for each computation, a program has been written by the authors which exploits the hard-wire capabilities of the  $\Sigma$ + key, computes MAD and range in addition to the other measures discussed, and stores the data for recall or transformation if desired. In addition, this program may be used with the TI 59 Master Module if the Statistics Module is not available. The following section describes the program in detail.

# 2. Univariate Data Program

In order to facilitate the description of this program a flow-chart (figure 4-1), has been included at the end of the chapter.

Comments in the paper are keyed to figure 4-1 by numbered circles for easy reference.

The program is initialized by pressing E' (figure 4-1,(1)). Initialization entails clearing all of the data registers, lowering flag 0 the purpose of which will be addressed later, and storing 31 in register 30. Register 30 is used as a post office for indirect addressing. In this particular program this means that data are stored in the register indicated by register 30. For example, after initialization, register 30 contains 31. The sequence  $\mathbf{x}_1$ , STO 2nd IND 30 will result in  $\mathbf{x}_1$  being stored in register 31. When the initialization routine, 2nd E', is complete the display will contain the value 31. Each datum may now be entered successively followed by pressing A. The routine at Label A begins by storing  $\mathbf{x}_1$  in a working, register 13 (figure 4-1,(2)).  $\mathbf{x}_1$  is then stored permanently beginning in register 31.  $\mathbf{x}_1$  is stored

in register 31, then register 30 the indirect storage address is incremented by 1 so that  $x_2$  will be stored in register 32,  $x_3$  in register 33 and  $x_n$  in register 31 + n - 1. A total of sixty-nine entries may be made using registers 31 through 99 for data storage. Registers 0 through 29 are used to make the requisite computations of central tendency and spread. After each datum,  $\boldsymbol{x}_{i}$ , has been stored, the program checks to see if flag 0 is raised (figure 4-1,(3)). If flag 0 is raised this indicates that a data entry has been made previously, ie., the current  $x_i$  is not  $x_1$ . In this event the program skips to Label x. If flag 0 is not raised, ie., the current  $x_i$  is  $x_1$ , then  $x_1$  is recalled from the working register, register 18, and stored in register 12 as the minimum  $\mathbf{x}_i$  and register 13 as the maximum  $\mathbf{x}_i$ . Future entries may then be checked against register 12 to determine which value is lower. If a current  $\mathbf{x}_i$  is lower than the value in register 12 then it will replace it as  $x_{min}$ . Similarly, subsequent entries may be checked against register 13 in order to retain  $x_{max}$ . After storing  $x_1$  in register 12 and in register 13 the program internally calls the key which, as disscussed previously, will sum  $\mathbf{x}_i$  into register 01, sum  $\mathbf{x_i}^2$  into register 02, sum the number of entries into register 03 and compute  $\overline{x}$ ,  $s^2$ , and MSD. Flag 0 is then raised so that subsequent entries will skip to Label x and replace  $x_{min}$  or  $x_{max}$  as appropriate. The program then recalls the number of entities, n, into the display and stops awaiting the next entry (figure 4-1, (4)). The second entry  $x_2$  will now be stored temporarily in the working register, register 18, and permanently in register 32. The indirect addressing register, register 30, is incremented by 1 for the next entry and the program then checks

to see if flag 0 is raised. Since this is not the first entry, the flag will be raised causing the program to skip to Label x (figure 4-1, (5)). The first step under Label x is to recall  $x_{min}$  from register 12 and store it in the test register  $R_T$ . For this particular iteration,  $x_1$ will be in register 12 since the first entry was both the maximum and the minimum value processed as described earlier. The program then recalls the current  $x_i$  ( $x_2$  in this instance) from the working register, register 18. The display value,  $x_2$ , is checked against the  $R_T$  value,  $\boldsymbol{x}_1^{}$  , to see if the display value is less than the  $\boldsymbol{R}_T^{}$  value. If so the program skips to step 57 where  $x_2$  is stored in register 12, replacing  $x_1$  as the lowest data entry (figure 4-1, (6)). If the display value is not less than the  $\rm R_{T}$  value then the program recalls  $\rm x_{max}$  from  $\rm R_{13}$  and stores it in  $R_{\mathrm{T}}$ .  $x_{\mathrm{i}}$  is recalled from the working register, register 18, into the display. This time the program checks to see if the display value,  $x_i$  is greater than the  $R_T$  value,  $x_{max}$ . If so, the program skips to step 62 where  $\mathbf{x}_i$  is stored in register 13 as the new  $\mathbf{x}_{\text{max}}$  (fig. 4-1, (7)). The program then computes the MIDVAL by recalling  $x_{min}$  from register 12 and  $x_{max}$  from register 13, summing them and dividing by 2, and storing in register 14. Next the range is computed by subtracting  $x_{\min}$  from  $x_{\max}$ . The range value is stored in register 15 (figure 4-1,(3)). The program then loops back to the + key to compute the mean, variance and MSD, (figure 4-1, 9). The number of entries is recalled and displayed awaiting the next entry. This process is repeated until all of the data have been processed.

The outputs of the program may be recalled as shown in table 3-11

in Appendix B. The mean is displayed by pressing  $\overline{x}$ , the variance by pressing Inv x, and MSD by pressing 2nd op 11. The lowest data point,  $x_{min}$ , may be discovered by recalling register 12 while the highest data entry,  $x_{max}$ , may be recalled from register 13. Recalling register 14 will display the MIDVAL and the range may be found by recalling register 15. Each of the original data entries may be recalled if desired beginning with  $\mathbf{x}_1$  in register 31. MAD is computed by pressing 2nd A' which calls a different subroutine. This subroutine recalls  $\overline{\mathbf{x}}$ which was computed under Label A and stores it in Register 16. The number of entries, n, is recalled from register 3 and stored in register 7 to be used as a decrement register. Register 20 contains 31 which is used to indirectly address the datum which have been stored beginning with register 31. The program recalls each x; using register 20 and subtracts  $\overline{\mathbf{x}}$ . The absolute value of the difference is summed into register 19. The program does this successively for each  $x_i$  until the decrement register, register 20, is equal to zero indicating that each  $x_i$  has been processed. The sum of the absolute values of the deviations from the mean is recalled from register 19 and divided by n which is recalled from register 3. This value, the mean absolute deviation is displayed completing the subroutine A' processing. All the values discussed earlier are still intact and may be recalled if needed. Table B-12, Appendix B, is a program listing for the univariate program.

# D. APPLICATION OF THE TI 59 UNIVARIATE PROGRAM

The cardiovascular scores for Category I provide a ready example for the use of the univariate program to calculate measures of central

tendency and spread. After the program card has been read in, the program is initialized by pressing 2nd E'. The cardiovascular scores for Category I (table 3-5) are entered into the calculator as follows: 56.5, A; 58, A; 58, A; 44.5, A; 33.5, A; 40, A. The instructions contained in table B-11 may then be used to obtain the desired statistics. For this particular example: 2nd x yields the mean, 48.4; RCL 14 displays the MIDVAL, 45.75; RCL 15 displays the range, 24.5; 2nd A' yields the mean absolute deviation, 9; 2nd Op 11 displays the mean squared deviation, 92.9; 2nd Op 11, $\sqrt{x}$ , calculates the root mean squared deviation, 9.6; INV 2nd  $\overline{x}$  recalls the standard deviation, 10.56; INV 2nd  $\overline{\mathbf{x}}$ ,  $\mathbf{x}^2$  calculates the variance 111.5; RCL 12 displays the lowest data entry, 33.5 and RCL 13 displays the highest data entry, 58. To calculate the sample statistics for another category or for a different test the user need only push 2nd E' to re-initialize and then enter the relevant data. Statistics have been calculated for the age, weight, cardiovascular scores, endurance scores, and strength scores for each of the six categories. Tables 4-1 through 4-6 display these statistics. Rather than discuss each of these tables in depth, one example is provided relative to the interpretation of the sample statistics.

The cardiovascular mean for Category I, 48.4, indicates average cardiovascular fitness using the Pipe's test which is based on a scale from 0 to 100. Three measures of spread (standard deviation 10.56, root mean squared deviation, 9.6, and mean absolute deviation, 9) are approximately equal to ten, a rather high variability in this case. The range, 24.5, also indicates that the data are quite spread out.

 $x_{\min}$  of 33.5 and  $x_{\max}$  of 58, the bounds of the sample data indicate that the cardiovascular fitness of sedentary people varies from poor to average.

Inferences, subject to the sampling limitations already discussed, may also be made about the strength or endurance of sedentary people using the data from table B-5. Similarly, the statistics for the other categories may be used to make inferences about the strength, endurance, or cardiovascular fitness of those who run over thirty miles per week (Category II) or those who lift weights (Category III) or any of the other three categories. Programs have also been written for the TI 59 which allow a user to develop confidence intervals for these sample statistics Ref. 14 .

The next chapter will discuss a program for one factor analysis of variance and then apply the program to the fitness data to illustrate statistical inference with the TI 59.

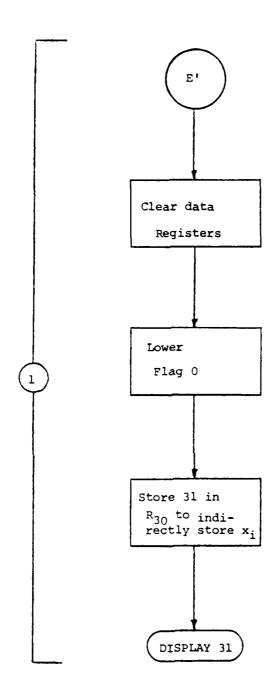


Figure 4-1.1

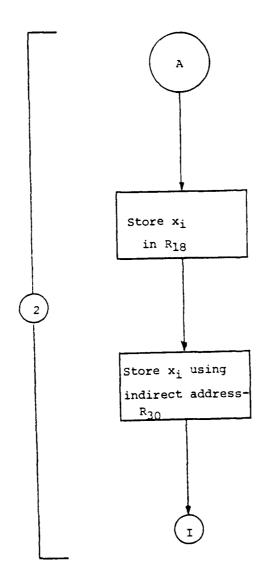
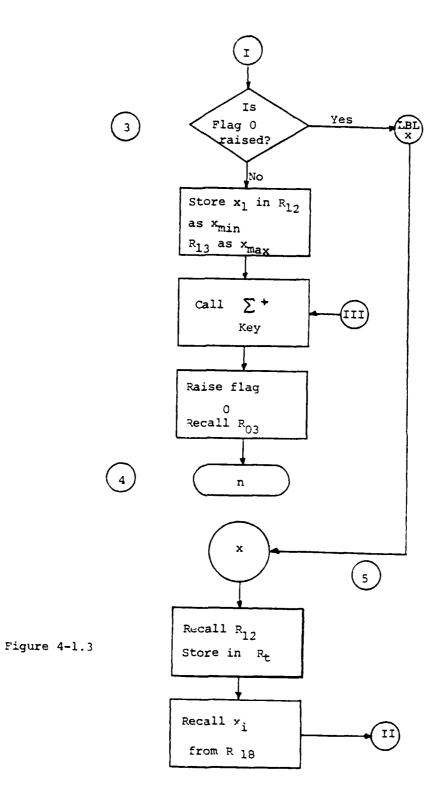
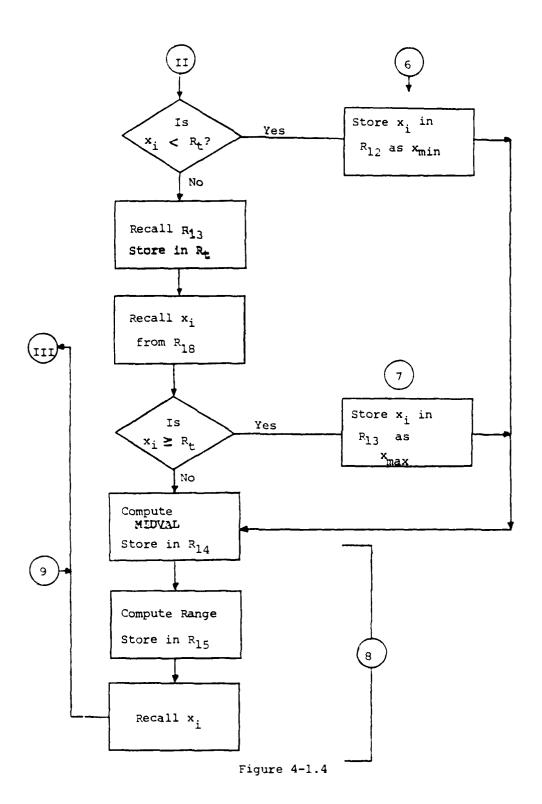


Figure 4-1.2





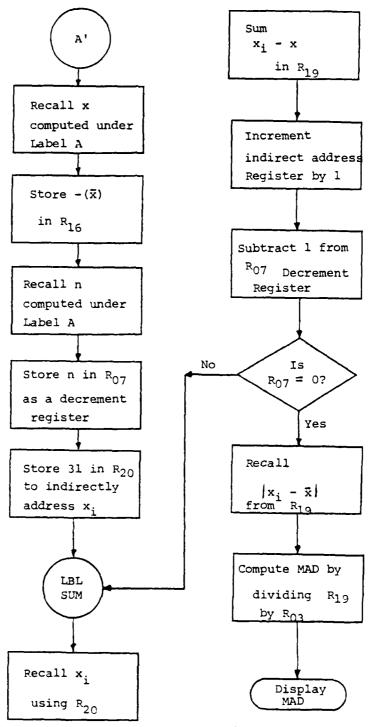


Figure 4-1.5

	MEAN	MIDVAL	RANGE	MAD	ر م	Ø	MSD	RMSD	Хмах	X min
33.3		33.00	8.00	2.30	0.6	3.00	7.5	2.74	37.0	29.0
172.8		180.00	50.00	16.40	412.0	20.30	345.1	18.58	205.0	155.0
<b>47°84</b>		45.75	24.50	00.6	111.5	10.56	92.9	09.6	58.0	33.5
1.17		1.15	.35	.085	.014	.12	.012	11.	1.32	.97
15.25		16.70	22.40	7.17	2.92	8.70	63.9	8.00	27.9	5.5

TABI,E 4-1

	MEAN	MIDVAL	RANCE	MAD	~బ	က	MSD	RMSD	X max	Xnin
AGE	32.2	31.5	2.0	2.11	96•9	2.6	5.8	2.41	35.0	28.0
WEICHT	164.5	161.0	68.0	16.16	529.0	23.0	6.044	20.99	195.0	127.0
CARD IO SCORE	4.58	75.75	41.5	10.4	229.9	15.16	191.6	13.8	96.5	55.0
STHENCTH SCORE	1.31	1.29	.36	.13	,026	.16	.022	.15	1.47	1.11
ENDURANCE SCORE	14.96	17.7	22,4	66.9	78.96	8.89	65.8	8.11	28.9	6.5

7<u>8</u>

Xmin	22.0	180.0	24.5	2.0	31.6
X max	34.0	225.0	86.5	2.83	62.5
RMSD	4.06	14.6	20.5	.065 .255	10.49
MSD	16.4	213.9	422.0	.065	110.0 10.49
Ø	4.115	16.0	22.5	.279	11.49
25	19.76	256.6	4.905	.078	132.0
MAL	×.	11.4	17.6	.20	9.3
HANGE	12.0	45.0	62.0	.83	30.9
MIDVAL	28.0	202.5	55.5	2.42	47.05
MEAN	26.8	205.3	52.25	2.39	917.917
	A(JE	WEIGHT	CA KD IO SCORE	STREN "TH SCORE	ENDURANCE SCORE

TAB1.E 4-3

X

19.0

160.0

D X max	32.0	240.0	96.5	7 2.67	0.64
RMSD	21.0 4.58	26.7	8.1	.27	4.9
MSD		714.6	65.3	20.	23.5
c3	5.02	29.3	8.85	.29	5.3
รู้ว	25.2	857.5	78•3	<i>t</i> 80.	28.2
MAD	3.67	21.67	6.9	.22	3.59
RANCE	13.0	80.0	25.0	χ. 21	41.65 14.2
MIDVAL	25.5	200.0	0.48	2,26	41.65
MEAN	28.0	187.5	83.4	2.23	141.38
	A 7E	WEICHT	CA KD IO SCORE	ЗТКЫМЛІН SCORE	ENDURANCE SCORE

30

1.85

34.3

71.5

X	19.0	120.0	39.5	1.15	22.0
X fiax	35.0	205.0	77.5	2.43	54.1
RMSD	5.6	26.0	11.8	.146 .38	12.2
MSI)	31.2	6.773	138.1	.146	148.8
$\infty$	6.1	28.5	12.9	.419	13.4
23 27	37.5	813.0	165.7	.176	178.6
MAD	7.4	19.3	8.2	.28	10.8
HA N. E.	<b>16.</b> 0	85.0	38.0	1.28	32.1
MIDVAL,	27.0	162.5	58.5	1.79	38.0
NEAN	7.82	171.5	55.8	1.83	34.4
	AGE	WEGSHT	CARD TO SCCRE	STREBATH SCORE	EWUTRANCE SCORE

TABLE 4-5

CATECORY VI STATISTICS

X min	22.0	125.0	47.5	1.15	11.4
X nax	33.0	205.0	86.5	1.56	23.1
KMSD	3.56 1.89	23.7	14.1	.016 .13	3.58
MSD	3.56	561.8	199.9	.016	12.8
က	2.06	25.96	15.5	.114	3.9
ಬ	4,26	674.2	239.9	.020	15,38
MA D	1.44	15.8	12.9	.11	2.83
HANGE	9.9	80.0	39.0	. 41	11.2
MIDVAL,	30.0	165.0	62.0	1.36	17.25 11.7
MEAN	2.08	170.8	6.05	1.36	16.6
	AGE	METARIA	CA hit I to SCORE	STRENUTH SCORE	ETILURANCE SCORE

∂2

## V. STATISTICAL INFERENCE

### A. PURPOSE

The purpose of this chapter is to illustrate a method of statistical inference using the TI 59. As in chapter IV the intent is to demonstrate the capabilities of the TI 59 rather than to emphasize statistical principles. One-way analysis of variance (ANOVA) will be used to demonstrate statistical inference using the fitness data discussed in the preceding chapter. The variations of the underlying populations represented by the six categories are assumed to be unknown but equal for this illustration.

## B. TI 59 PROGRAM FOR ANALYSIS OF VARIANCE

In testing the hypothesis that the population means for each of the six test categories are equal,  $H_0$  is typically rejected if the F ratio exceeds the critical F value in a standard table for the desired test level (typically 5%). Alternatively, using the TI 59 to its full advantage, prob-value may be used to test  $H_0$ . Prob-value is a method of testing whether or not the null hypothesis is supported by the data. In the case of the F ratio, prob-value is the probability that the F ratio would be as large or larger than the value actually observed if  $H_0$  were true. This is the right hand tail area, Q (f), where

$$Q(f) = Pr (F > f)$$

prob-value has the advantage that analysis is not restricted to arbitrarily established test levels such as 5% or 10% or to use of standard published tables. The TI 59 Statistics Module has an F distribution program (Program 22) which computes the tail area of an F curve where

the curve is defined by the degrees of freedom in the numerator and the denominator. A series expansion is used to approximate the integral to determine Q(f) [Ref. 10]. If  $H_0$  is true, indicating that all of the observations are from the same normal population, then the prob-value, Q(f), will be large. Conversely, if  $H_0$  is false then the prob-value will be small. If the prob-value is sufficiently small (as determined by the decision-maker) then  $H_0$  is rejected and the conclusion is formed that there must be a difference in the population means somewhere [Ref. 14].

While a classical test or prob-value may facilitate rejection or acceptance of the null hypothesis, no insight is provided as to which means differ, given that H<sub>0</sub> is rejected. There is an efficient method developed by Sheffe Ref. 13 for computing confidence intervals for the difference between means. If the physical fitness example discussed earlier is used, then Sheffe's development may be used to make the following statements with 95% confidence:

$$(\mu_{1} - \mu_{2}) = (\overline{X}_{1} - \overline{X}_{2}) \pm \sqrt{(r-1)F_{.os}} S_{p} \sqrt{\frac{1}{D_{1}} + \frac{1}{D_{2}}}$$

$$(\mu_{1} - \mu_{3}) = (\overline{X}_{1} - \overline{X}_{3}) \pm \sqrt{(r-1)F_{.os}} S_{p} \sqrt{\frac{1}{D_{1}} + \frac{1}{D_{3}}}$$

$$(\mu_{2} - \mu_{3}) = (\overline{X}_{2} - \overline{X}_{3}) \pm \sqrt{(r-1)F_{.os}} S_{p} \sqrt{\frac{1}{D_{2}} + \frac{1}{D_{3}}}$$

Where  $F_{.05}$  is the critical value of F which leaves 5% in the upper tail,  $S_{\rm p}$  is the square root of the pooled variance, r is the number of means

compared, and n is the size of each of the samples. In the fitness example this equates to making confidence statements about the difference in fitness between the six categories where r is six and n is 6 for each of the samples. To facilitate multiple comparisons a contrast of means is used. This contrast may be written as:

$$\sum C_i \mu_i$$
 where  $\sum C_i = 0$ 

It is then possible to develop the following formula which includes all possible contrasts with 95% confidence:

$$\sum c_i \mu_i = \sum c_i x_i \pm \sqrt{(r-i) F_{os}} S_p \sqrt{\sum \left(\frac{C_i}{n_i}\right)^2}$$

If the value 0 is included in a confidence interval then there is no basis for believing that the population means differ while if 0 is not included then the conclusion is drawn that the means do in fact differ.

A program has been developed by Dr. P.W. Zehna Ref. 14 for the TI 59 which computes the elements of an ANOVA table (table B-15)to include the F ratio and prob-value discussed above. Basically the program exploits the TI 59 F distribution program for determining prob-value (Program 22) after using Program 15 of the Statistics Module Ref. 10 to calculate the F statistic. The program then uses Scheffe's multiple contrasts to determine which population means differ given that the null hypothesis is rejected.

A flowchart (figure 5-1), user instructions (table B-13), and a listing of the actual program steps (table B-14) are provided to facilitate description of the ANOVA program. The program takes data input by rows and outputs the elements of an ANOVA table (table B-15) sequentially

as indicated by the number in each block of the table. A row of data constitutes a sample as in the example at table B-16.

The program begins by using Program 06 of the Statistics Module to enter the data. After initialization with 2nd E' each  $\mathbf{x}_{i,j}$  is entered followed by pressing Label A. When one complete row has been entered a press of 2nd B' causes the calculator to compute the row or sample x and a press of 2nd C' results in computation of the MSD. These two steps must be performed after each row has been input so that the calculator will know when a new row is being entered. When all of the data have been entered using this scheme (table B-13) the sequence RST, A begins the ANOVA Table calculations. The first step under Label A is to call Program 15 of the TI 59 Statistics module which computes the F ratio. In the process of computing the F ratio the other elements of the ANOVA table (table B-15) are computed and stored except for the prob-value. To fill in the values for the ANOVA table all that is required is successive pushes of R/S as indicated in table B-13. For example, the first R/S displays the degrees of freedom for the numerator while the fourth R/S displays the degrees of freedom for the denominator. The program essentially recalls and displays the calculations of Program 15 of the Statistics Module to build the ANOVA table. To compute probvalue the program internally calls Program 22 of the Statistics Module. The user need only press R/S as indicated in table B-13 which causes the calculator to recall the degrees of freedom for the numerator and the denominator used in Pgm 15 and transfer them to Program 22 to define the F Distribution. The F statistic calculated in Program 15 is then

recalled and transferred to Program 22 resulting in  $\Omega(f)$ , the probability that F > f. This prob-value may then be used to accept or reject the null hypothesis. If the null hypothesis is accepted then the analysis is completed. However, if  $H_0$  is rejected, the next step entails the use of Scheffe's contrasts to determine which means differ.

To use the ANOVA program (table B-14) for posterior contrasts with Scheffe's formulas the user initializes the routine by pressing 2nd E'. Then  $c_i$ ,  $x_i$  and  $n_i$  are entered for each row as shown in table B-13. The  $c_i$ 's are the coefficients used to determine which means are contrasted as discussed previously. To contrast  $u_1$  and  $u_2$ ,  $c_1$  = 1,  $c_2$  = -1 and all other  $c_i = 0$ . To contrast  $u_2$  and  $u_3$ ,  $c_2 = 1$ ,  $c_3 = -1$  and all other  $c_i = 0$ . As these data are input, the program uses a 'loop' to calculate which is stored in register 03 and  $\sum C_i X_i$  which is stored in register 06, (figure 5-1). Register 04 is used as a counter to display the number of row entries. After each  $c_i$ ,  $x_i$  and  $n_i$  entry, register 04 is incremented by one. The program then transfers to Label  $x^2$ , displays the running count of row entries and stops pending the next entry. After every  $c_i$ ,  $x_i$  and  $n_i$  have been processed, a critical value of F with degrees of freedom r-l and n(r-l) is entered for the desired test level followed by 2nd A'. The program recalls the degrees of freedom for the numerator, r-1, from register 14 and the pooled variance  $S_p^2$  from register 29. The product  $(r-1) F_2 S_p^2$  is formed and multiplied by the contents of register 03  $\sum \left(\frac{C_i}{D_i}\right)$  . The square root of this product is stored in register 05. This value is then added to and subtracted from the contents of register 06,  $\sum c_i x_i$ , to form the desired

confidence interval. The lower bound is displayed after the use of 2nd A' and the upper bound may be recalled by pressing R/S (table B-13).

An example will now be provided using this program to test for differences between population means for the fitness experiments.

## C. APPLICATION OF THE TI 59 ANOVA PROGRAM

The null hypothesis, H<sub>Q</sub>, may be stated as - there is no difference in the cardiovascular fitness of those who do no exercise (Category I), those who run in excess of thirty miles per week (Category II), those whose exercise consists solely of lifting weights (Category III), those who lift weights and run in excess of twenty miles per week (Category IV), those who lift weights and run between ten and nineteen miles per week (Category V), and those who do not run or lift weights but participate in other activities such as basketball, racquetball or bicycling (Category VI). Table B-35 reflects the cardiovascular score for each of the thirty-six subjects tested by category as well as the mean for each category. The null hypothesis that there is no difference between these category means may be tested using the ANOVA program with each of the categories constituting a row for input.

After the program card has been read in, the ANOVA program is used by first calling program 06 of the statistics module to enter the data. After initialization with 2nd E', the data for each row are entered followed by A. For the cardiovascular scores (table B-35) the first row, Category I, would be entered as follows: 56.5, A; 58, A; 44.5, A; 33.5, A; 40, A. Once the row data have been entered 2nd B' is pressed to display the row mean, 48.4, followed by C' which displays

the row MSD, 92.9. (The row mean must be recorded for use in posterior contrasts). The data are then entered in a similar fashion for the remaining five rows (Categories II through VI). Once all of the data have been entered, RST is pressed to return the calculator pointer to the ANOVA program. A is then pressed resulting in calculation of the ANOVA Table entries. The ANOVA entries are recalled with sequential presses of R/S. Table B-13 discussed earlier contains detailed instructions on the use of the ANOVA program. Table 5-1 depicts the ANOVA calculations for the cardiovascular scores of the six fitness test categories. The prob-value of .00027 is sufficiently small to cast doubt upon the null hypothesis that there is no difference in the cardiovascular fitness among the six categories tested.

As discussed previously, the prob-value tells how credible the null hypothesis is but it does not tell which categories differ given that there is cause to reject  $H_0$ . However, confidence intervals may be established for contrasts between the categories using Scheffe's formula which is programmed in the ANOVA routine  $\begin{bmatrix} Ref. & 13 \end{bmatrix}$ . For the cardiovascular example, the cardiovascular fitness of the sedentary subjects (Category I) may be contrasted to the cardiovascular fitness of the runner (Category II) as a demonstration of the program. 2nd E' is pressed to initialize the contrast routine followed by  $c_i$ ,  $x_i$  and  $n_i$  for each of the two rows. For Categories I and II the entries are:

l R/S 48.4 R/S 6 R/S

<sup>-1</sup> R/S 83.4 R/S 6 R/S

The appropriate F percentile is entered followed by A' to generate the desired confidence interval. To display a 95% confidence interval for the difference in cardiovascular fitness between Categories I and II an F percentile of 2.53 (where there are five degrees of freedom in the numerator and thirty degrees of freedom in the denominator) is used resulting in an interval from -65.5 to -41.4. Since 0 is not included in the interval it is reasonable to conclude that there is a difference in the cardiovascular fitness of the two categories. Table 5-2 contains the results of contrasting each of the six fitness categories. Only four contrasts result in the conclusion that there is a difference between the categories with 95% confidence: Category I - Category II (-65.5, -41.4); Category I - Category IV (-65.5, -4.4); Category II -Category III (.6, 61.8) and Category III - Category IV (-61.7, -6.0). These results indicate with 95% confidence that there is a difference in the cardiovascular fitness of those who run more than twenty miles per week (Categories II and IV) and those who do no running at all (Categories I and III), at least for those subjects examined.

The ANOVA program has also been applied to the strength and cardiovascular scores resulting from the experiment. Table B-36, Appendix B, reflects the strength scores of each of the thirty-six subjects by category. The ANOVA results are contained in Table 5-3. The prob-value of .12 x 10<sup>-8</sup> indicates that the null hypothesis that there is no difference in the strength of members of the different categories should be rejected. Further analysis with posterior contrasts is necessary to see which categories differ. Table 5-4 contains the results of posterior contrasts with an F percentile of 2.53 for 95%

confidence with five and thirty degrees of freedom for the numerator and denominator respectively. Unlike the cardiovascular contrasts there are a number of differences in the strength results. Categories III and IV, which were composed of the most ardent weightlifters, differs from Categories I and III but not VI. These results are not surprising in that they confirm the hypothesis that different training programs result in different levels of fitness. In this instance where fitness is defined as strength, those who trained for strength were in fact stronger than those who did not. Again, without attempting inference to a larger population, these results may be used to gain insight into the probable differences that might be tested in a more appropriately designed experiment.

Table B-37, Appendix B depicts the endurance scores for the thirty-six subjects by category. Table 5-5 reflects the results of using the ANOVA program with the endurance scores as input. Once again, the prob-value of .137 x 10<sup>-6</sup> indicates rejection of the null hypothesis (in this case that there is no difference in the upper body endurance of the members of the six different categories). The posterior contrasts (table 5-6) indicate that the weightlifters (Categories III, IV, V) differ from the non-weightlifters (Categories I, II, VI) in upper body endurance with 95% confidence. This also supports the hypothesis that different training programs result in different levels of fitness, subject again to the sampling restrictions previously discussed.

## D. SUMMARY

While the results of the fitness experiment are interesting, the purpose of this analysis has been to demonstrate a statistical application of the TI 59 and not draw inference to a hitherto undefined population. The univariate program was used to calculate measures of central tendency and spread for the Category I Cardiovascular scores. The ANOVA program was used to test for differences in strength, endurance, and cardiovascular fitness among the six test categories. In both instances meaningful but guarded inferences were drawn from the test data.

The capabilities of the TI 59 in real world statistical analysis are impressive. The analyst can conduct sophisticated analysis of good-sized samples unconstrained by access to large computers. Using programs such as those demonstrated in this chapter the analyst need not even learn a programming language. All that is required to compute an F ratio or prob-value, for example, is the ability to follow simple users' instructions. While there are certainly samples whose size preclude the use of the TI 59, there are a pletheora of samples which can be analyzed more conveniently and just as efficiently at home or at the office using the TI 59.

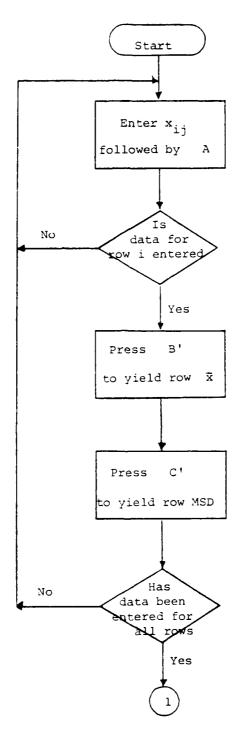


Figure 5-1.1

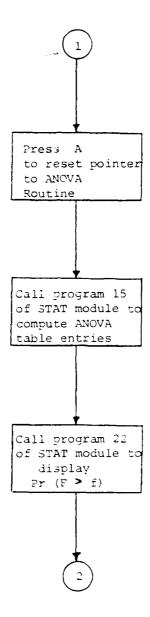


Figure 5-1.2

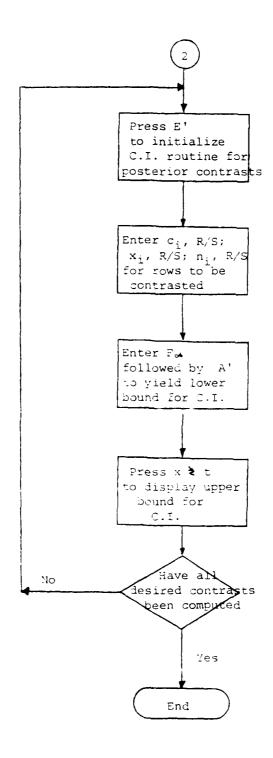
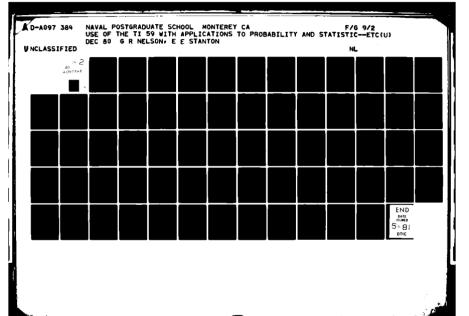


Figure 5-1.3



# CARDIOVASCULAR ANOVA TABLE

VARIANCE

$$\begin{array}{ccc} & & & r \\ n & & & \Sigma \\ & & & 1=1 \end{array} \left( \ddot{x_1} - \ddot{x} \right)^2 \\$$

$$\frac{100}{x}$$

(r-1)

3 1478.3

(2) 5.00

(I) 7391.6

$$\begin{array}{ccc} \mathbf{r} & \mathbf{n} \\ \Sigma & \Sigma & (\mathbf{x_{1j}} - \bar{\mathbf{x}_{1}})^{2} & \mathbf{r(n-1)} \\ \mathbf{1} & \mathbf{j} & \end{array}$$

$$\sum_{\mathbf{j}}^{\mathbf{n}} (\mathbf{x}_{\mathbf{1}\mathbf{j}} - \bar{\mathbf{x}}_{\mathbf{1}})^2$$

5 30.0

0.0999 🕀

$$\sum_{i} \sum_{j} (x_{i,j} - \bar{x})^2 \qquad (nr - 1)$$

TOTAL

$$(nr - 1)$$

9	-53.1 8.1	-18.1 43.1	-49.2 11.9	-18.1 43.1	-45.7 15.5
5	-37.9 23.2	- 2.9 58.2	-34.2	- 2.9	
4	-65.5 - 4.4	-30.6 30.6	-61.7 - 6.0		
3	-34.3	.6 61.8			
8	-65.5 -41.4				
1					
		8	8	7	۸.

TABLE 5-2

9

## STRENGTH ANOVA TABLE

SUM OF	SQUARES
SOURCE OF	/ARIATION

BETWEEN 
$$n = \sum_{1=1}^{r} (\bar{x}_1 - \bar{x})^2$$
 ROWS

$$(r - 1)$$

③ 1.5%

(2) 5.00

(1) 7.98

$$\begin{array}{ccc} \mathbf{r} & \mathbf{n} \\ \Sigma & \Sigma & (\mathbf{x_{1j}} - \bar{\mathbf{x_{1}}})^2 \\ \mathbf{1} & \mathbf{j} & \mathbf{x_{1j}} - \bar{\mathbf{x_{2}}})^2 \end{array} \quad \mathbf{r(n-1)}$$

(5) 30.00

(t) 1.99

S2 d

$$\sum_{i} \sum_{j} (x_{i,j} - \bar{x})^2 \qquad (nr - 1)$$

## TABLE 5-3 .

99

SOURCE OF VARIATION

VARIANCE

F RATIO

PROB-VALUE

BETWEEN ROWS

 $\begin{array}{ccc}
\mathbf{r} & \mathbf{r} \\
\mathbf{n} & \mathbf{\Sigma} & (\mathbf{x_1} - \mathbf{x})^2 \\
\mathbf{1} = \mathbf{1} & \end{array}$ 

(r-1)

(3) 1329.92

(2) 5.00

19.6499.(1)

(10)  $.137 \times 10^{-6}$ 

 $\begin{array}{ccc} \mathbf{r} & \mathbf{n} \\ \Sigma & \Sigma & (\mathbf{x_{1j}} - \bar{\mathbf{x}_{1}})^{2} & \mathbf{r(n-1)} \\ \mathbf{1} & \mathbf{j} & \end{array}$ 

WITHIN ROWS

(4) 2549.41

(5) 30.00

®.¥ ⊚

9 15.65

32 P

TOTAL

 $\begin{array}{ccc} \Sigma & \Sigma & (x_{1j} - \bar{x})^2 & (nr - 1) \\ i & j & \end{array}$ 

(7) 9199.05

8 35.00

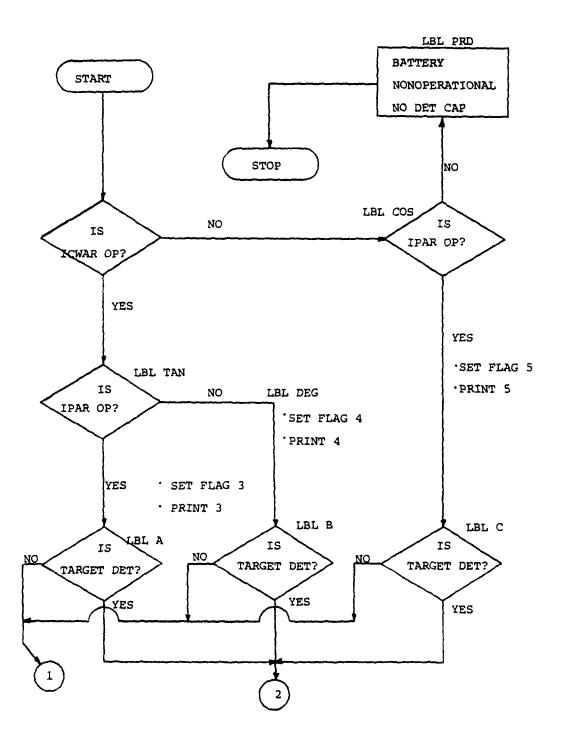
TABLE 5-5

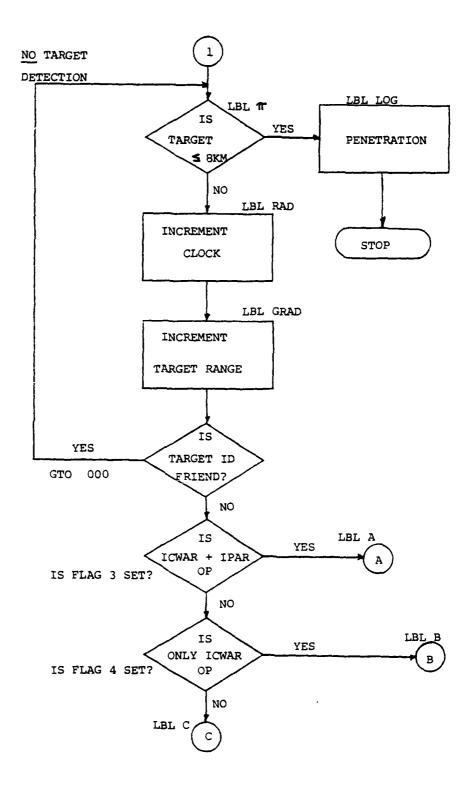
## APPENDIX A

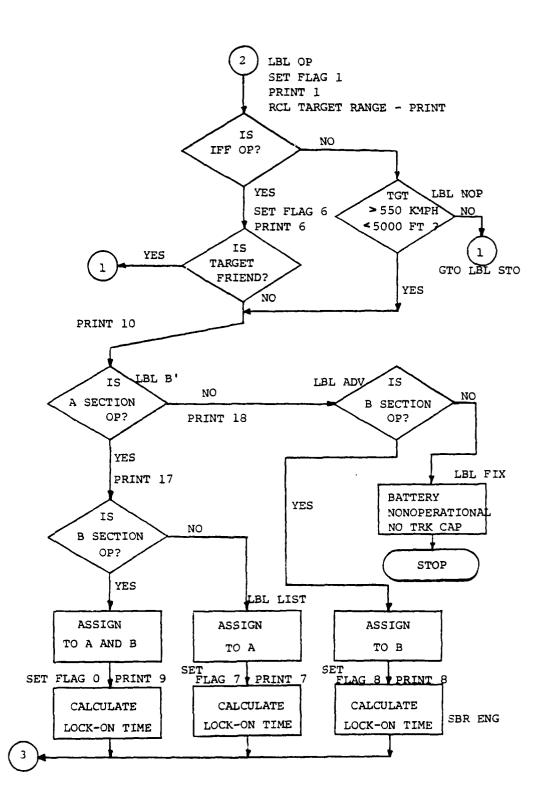
## COMMENTS ON SELECTED LABELS

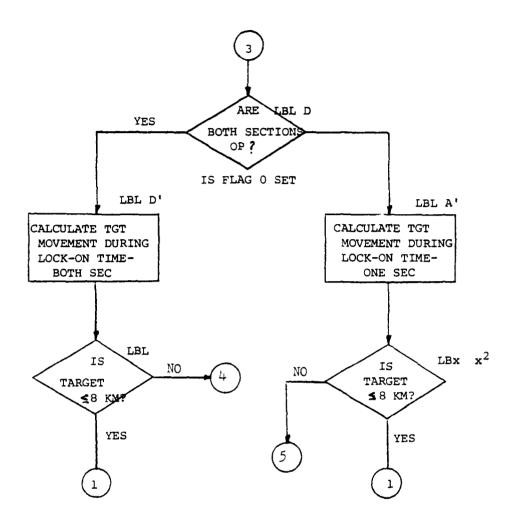
LABEL	COMMENT
A	Directs action to compute glimpse probability of detection for both ICWAR and IPAR
x	Computes glimpse probability of detection for ICWAR only based on target range
$\overline{\mathbf{x}}$	Computes glimpse probability of detection for IPAR only based on target range
E and LnX	Determines if target is less than 40 KM from unit and directs processing accordingly.
ים'	Calculates target range after elapse of target lock-on time.
(SBR) EXC a	nd INT Increments range of IHAWK missile after firing
FIX	Prints 24 (no firing capability)
DSZ	Prints 14 (cruise missile identified as friend)
NOP	Prints 66 (IFF is nonoperational)
OP	Prints 1 (target detected) at range (KM), begins engagement sequence
(SBR) RAD a	nd $y^x$ Increments simulated air battle time clock $(R_{19})$ .
(SBR) GRAD	and $\frac{1}{X}$ Computes cruise missile rate of approach and increments target range (R <sub>00</sub> ).
(SBR) ENG	Random number generation - normal distribution
(SBR) P→R	Random number generator - uniform distribution
PRD	Prints 23 (no detection capability)
sin	Prints "KILL" and range of target kill
LOG	Prints "PENETRATION"
(SBR) WRITE	AND $\pi$ Prints "PENETRATION" if target is 8 KM or less

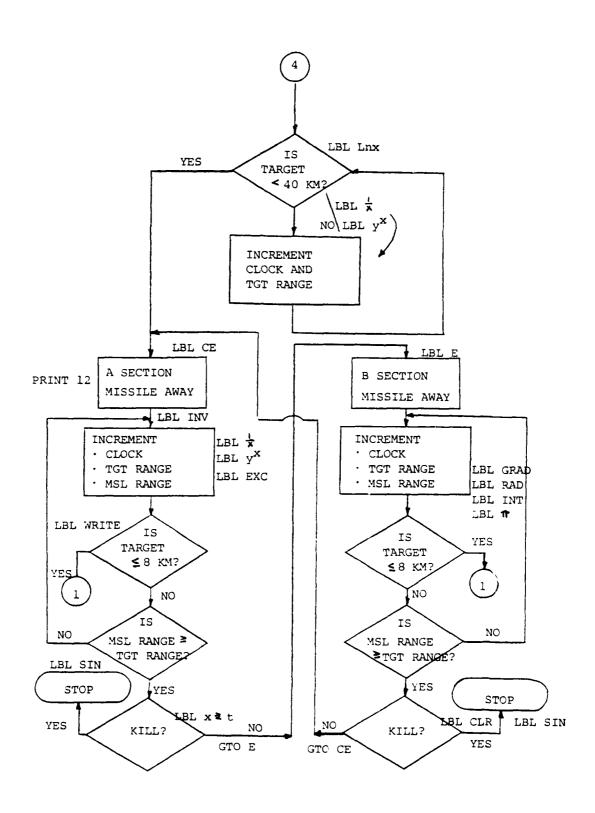
from unit.

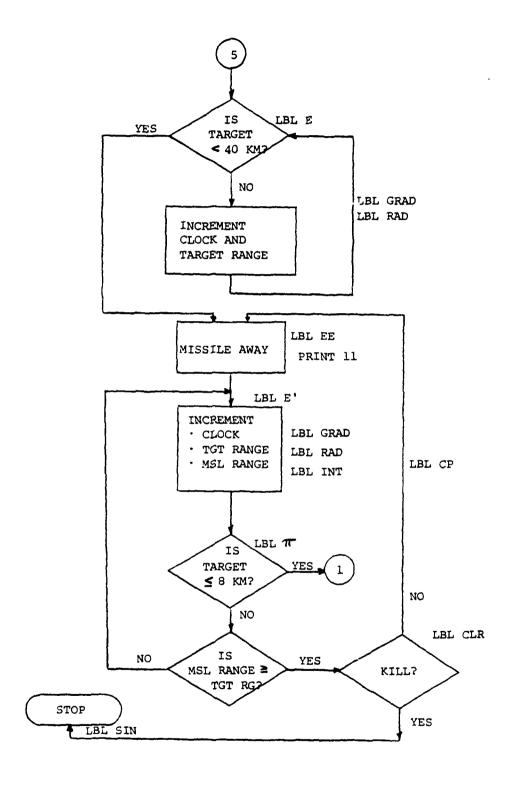












#### SIMULATION PROGRAM

000 001	71 SBR 89 .1		041 042	<b>05</b> 5 99 PRT
002 003	71 SBR 80 GRD		043 044	13 C 76 LBL
004 005	71 SBR 70 RAD		045 046 047	30 TAN 71 SBR 37 P/R
006 007 008	87 IFF 02 02 00 00	i	048 049	93
009 010	00 <b>00</b> 87 IFF		050 051	09 9 05 5 32 X <b>:</b> T
011 012	03 03 11 A		052 053 054	77 GE 60 DEG 86 STF
013 <b>01</b> 4 015	87 IFF 04 04 12 B		055 056	03 03
016 017	87 IFF 05 05	;	057 058	03 3 99 PRT 11 A
018 019	13 C 71 SBR	,	059 060 061	76 LBL 60 DEG 86 STF
020 021 022	37 P/R 93 . 06 6		062 063	04 04 04 4
023 024	05 5 32 X:T	ť.	064 065	99 PRT 12 B 76 LBL
025 026 027	77 GE 39 COS 61 GTO		066 067 068	69 <b>O</b> P
027 028 029	30 TAN 76 LBL		069 070	99 PRT 43 RCL
030 031	39 COS 71 SBR	,	071 072 073	00 00 99 PRT 71 SBR
032 033 034	93 .	: -}	073 074 075	37 P/R
035 036	05 5 32 X∶T	-	076 077	09 9 05 5
037 038	77 GE 49 PRD		078 079 080	32 X∤T 77 GE 68 NOP
039 040	86 STF <b>05</b> , 05	, a	081	06 6

THIS PAGE IS BEST QUALITY PRACTICATED.

SHOW COPY FORMISMED TO BEG

```
123
                                 71 SBR
082
      99 PRT
                           124
                                 57 ENG
083
      86 STF
                           125
                                 32 X:T
084
     06
         -06
                           126
                                 42 STO
085
      71 SBR
                           127
128
                                  14
                                     14
      37 P/R
086
                                 71 SBR
087
      93
          98
                           129
                                 57 ENG
088
     09
                           130
131
                                 32 X:T
089
     08
090
      32 X1T
                                  42 STO
                           132
091
      77
                                 08
                                     - 08
         GE
     97 DSZ
                                 18 C.
                           133
092
093
                           134
                                 76 LBL
      01
         1
094
                           135
                                 98 ADV
      00
          0
                           136
                                     1
                                 01
095
      99 PRT
                           137
                                 08
                                      8
096
      61 GTO
                           138
                                 99 PRT
097
      17 B*
                           139
                                 71 SBR
      76 LBL
098
      17 B*
                           140
                                 37
                                     P/R
099
                                     .
7
5
                            141
                                 93
      71 SBR
100
                           142
                                 07
101
      37 P/R
                           143
                                 05
102
      93
          7
                                 32
77
                                     XIT
                           144
103
      07
104
      05
         - 5
                           145
                                      GE
      32 X:T
                           146
                                  58 FIX
105
                           147
                                  08
                                     8
106
      77
         GE
      98 ADV
                           148
                                  99 PRT
107
                            149
                                  86 STF
108
      01
          1
                            150
                                  08
                                      -08
109
      07
                            151
                                  71 SBR
110
      99 PRT
                           152
153
                                 57 ENG
      71 SBR
111
                                  32 X:T
      37 P/R
112
113
                            154
                                 42 STO
      93
          7
                           155
                                  08
                                     08
114
      07
                                  18 C'
                           156
         5
115
      05
      32 X:T
                           157
                                  76 LBL
116
                           158
159
                                  90 LST
      77
117
          GΕ
                                  07
118
      90 LST
                            160
                                  99 PRT
119
      09
          9
                                  86 STF
120
      99 PRT
                            161
                                  07
                                      07
121
      86 STF
                            162
                            163
                                  71
                                     SBR
122
           00
      00
```

MAIS PAGE IS BEST QUALITY PRANTICARY

```
205
                                OO
164
      57 ENG
                                19 D'
                          206
      32 X:T
165
                       207
208
                                76 LBL
      42 STO
166
                                16 A'
167
      08 08
                                   (
                         209
                                53
168
      18 C'
                          210
                               43 RCL
169
      76 LBL
                          211
                                08
                                   - 08
170
      42 STO
                          212
                                   ÷
                                55
171
      86 STF
                       213
214
                                03
                                   3
172
173
      02 02
                                85
         1
      01
                          215
                                93
      05 5
174
                          216
                                05
                                    5
175
      99 PRT
                          217
                                54
                                   )
      61 GTO
176
                          218
                               59 INT
177
      00 00
                          219
                               42 STD
178
      00 00
                       220
                               04
                                   04
179
      76 LBL
                          221
                                76 LBL
      18 C'
180
                          222
                                43 RCL
181
      87 IFF
                                71 SBR
                          223
182
      06 06
     14 D
05 5
00 0
                          224
                                80 GRD
183
                          225
                                71 SBR
184
                          226
227
                                70 RAD
185
                                97 DSZ
      00 0
00 0
186
                          228
                                04
                                   04
187
                         229
                                43 RCL
188
      32 X:T
                         230
                                76 LBL
 189
      43 RCL
                          231
                                33 X2
 190
      16 16
                          232
                                71 SBR
 191
      77 GE
                          233
                               89 1
 192
      42 STO
                       234
                                76 LBL
 193
      05 5
                          235
                                15 E
      05
 194
          5
                          236
                                04
                                   4
 195
         n
      00
                          237
                                   0
                                00
 196
      32 X:T
                          238
                                32 X:T
 197
      43 RCL
                                43 RCL
                          239
 198
      15 15
                          240
                                00 00
      22 INV
 199
                          241
                                22 INV
 200
      77
         GE
                          242
                                77
                                   GE
      42 STD
 201
                          243
                                52 EE
 202
      76 LBL
                          244
                                71 SBR
 203
      14 D
                          245
                                80 GRD
204, 87 IFF
```

THUS PAGE IS REST QUALITY PRACTICANANT FROM SOUTH STREET OF THE PROPERTY OF TH

```
287
                                  05
     71
246
         56R
                                  43 RCL
                            288
247
      70 RAD
                            289
                                  00
                                     00
248
     61 GTD
                            290
                                  42 STD
249
      15
         Ε
                            291
                                  17
                                     17
250
     76 LBL
                            292
                                  43 RCL
251
      52 EE
                            293
                                  19
                                      19
252
      87
         IFF
                            294
                                  42 STO
253
      07
         - 07
                            295
                                  01
                                     01
      44 SUM
254
                            296
                                  76 LBL
255
      01
         1
                            297
                                  67
                                     EQ
256
      01
         1
                            298
                                  71 SBR
257
      99 PRT
                            299
                                  35 1/X
258
      76 LBL
                                  71 SBR
259
      10 E'
                            300
                                  45 YX
                            301
260
      71 SBR
                            302
                                  97 DSZ
261
      80 GRD
                            303
                                  05
                                      -05
      71 SBR
262
                            304
                                  67
                                       EŪ
263
      70 RAD
                            305
                                  53
                                     (
      71 SBR
264
                                  43 RCL
                            306
      59 INT
265
                            307
                                  08
                                      -08
      71 SBR
266
                            308
                                  55
267
      89
          1Î
                            309
                                  03
268
      43 RCL
                            310
                                  85
                                       +
269
      00
         00
                                  93
                            311
270
      32 X:T
                            312
                                  05
271
      43 RCL
                            313
                                  54
                                       )
272
      12
          12
                                  59 INT
273
274
      77
                            314
          GE
                                  42 STO
      25 CLR
                            315
                                  04
                            316
                                     04
275
      61 GTO
      10 E'
                            317
                                  76 LBL
276
277
                            318
                                  88 DMS
      76 LBL
                           .319
                                  71 SBR
278
      19 D'
                                  80 GRD
         (
                            320
279
      53
                                  71 SBR
      43 RCL
                            321
230
                            322
                                  70 RAD
          14
281
      14
                            323
                                  97 DSZ
282
      55
           3
                            324
                                  04
                                       04
283
      03
          > .....
                                  88
                                     DMS
                            325
284
      54
                            326
                                  43 RCL
285
      59 INT
                            327
                                  17
                                       17
      42 STO ......
286
```

THIS PARK IS BUST QUARTET PRACTICANA

```
369
                                    17 E'
328
      32 X:T
329
      43 RCL
                              370
                                    32 X:T
                                    43 RCL
                              371
330
      00
          -00
331
332
333
                              372
      77
         GE
                                    13
                                        13
      33 X2
                              373
                                    77
                                         GE
                              374
                                    32 X:T
      76 LBL
                              375
334
      34 FX
                                    61 GTD
335
336
337
338
339
                              376
      71 SBR
                                    22 INV
                                    76 LBL
                              377
      96 WRT
                              378
                                    32 X:T
      76 LBL
                              379
                                    71 SBR
      23 LNX
                              380
                                    37 P/R
      04
         4
340
                              381
      00
          0
                                    93
                                        .
7
5
                              382
                                    07
341
      32 X∶T
                              383
342
      43 RCL
                                    05
343
344
345
      17
                              384
                                    32 X:T
          17
                              385
                                    22 INV
      22 INV
      77 GE
                              386
                                    77
                                       GE
      24 CE
346
                              387
                                    38 SIN
                                    71 SBR
78 Z+
                              388
347
      71 SBR
                             389
348
      35 1/X
349
                             390
                                    61 GTD
      71 SBR
                             391
      45 YX
350
                                    15 E
351
                             392
                                    76 LBL
      61 GTD
                                    25 CLR
                             393
352
      23 LNX
353
354
355
356
357
358
                             394
                                    71 SBR
      76 LBL
                             395
                                    37 P/R
      24 CE
                             396
397
                                    93
07
      01 1
                                         .
7
5
      02 2
                             398
399
400
                                    05
      99 PRT
                                    32 X:T
      76 LBL
359
360
                                    22 INV
77 GE
      22 INV
                             401
      71 SBR
                             402
361
      35 1/X
                                    38 SIN
362
      71 SBR
                             403
                                    71 SBR
                                    29 CP
                             404
363
      45 YX
                             405
                                    87 IFF
364
      71 SBR
      48 EXC
                             406
                                    00
                                         00
365
                             407
                                    34 JX
366
      71 SBR
      96 WRT
                             408
                                    61 GTD
367
                             409
                                    15
368
     43 RCL
```

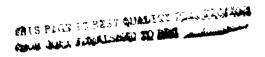
```
410
      76 LBL
                               451
                                     61 GTD
411
      28 LOG
                               452
                                     07
                                          07
412
413
      25 CLR
                               453
                                     72
                                           72
      69 DP
                               454
                                     76 LBL
414
415
416
      00
          0.0
                               455
                                     38 SIN
                                     25 CLR
            3
      03
                               456
            3
      03
                               457
                                     69 OP
417
      69 OP
                               458
                                     00
                                          00
418
      01
          01
                               459
                                     69 DP
419
420
      01
            1
                               460
                                     01
                                          01
      07
            7
                               461
                                          2
                                     02
421
           3
      03
                               462
                                          6
                                     06
                                          24
422
      01
           1
                               463
                                     02
423
424
425
426
427
                               464
           17373
      01
                                     04
      07
                               465
                                     69 OP
      03
                               466
                                     02
                                          02
                                     02
                                          27
      07
                               467
      03
                               468
                                     07
                                          2
7
428
      05
           5
                               469
                                     02
429
      69
          DF
                               470
                                     07
430
      02
                                          Ū
          02
                               471
                                     00
                              472
473
431
      01
           1
                                     00
                                          0
           4007Q40
432
433
      03
                                     00
                                          0
      03
                               474
                                          0
                                     00
434
435
436
      07
02
                              475
476
                                          0
                                     00
                                     00
                                          0
                              477
478
      04
                                     69 OF
           3223
      03
02
437
                                     03
                                          03
438
                              479
                                     00
                                          0
439
      03
                              480
                                     69 DP
440
                              481
          1
      01
                                     04
                                          04
441
                              482
      69 DP
                                     69 OP
442
443
                              483
      03
         03
                                     05 05
      00
                              484
                                     43 RCL
           0
                              485
486
487
444
      69 DP
                                     00
                                         00
445
      04
           04
                                     99 PRT
446
      69 OP
                                     61 GTD
447
      05 05
                              488
                                     07
                                          07
                                     72
448
      43' RCL
                              489
                                          72
449
      18
          18
                              490
                                     76 LBL
450<u>99</u> PRT
                                     37, P/R
                              491
```

493 15 18 22 19 15 18 15 19 15	15 GM 15 BM 17 BM 17	3456789012345678901234567890123456789 555555555555555555555555555555555555	00 LB 8 0 0 0 T L6 E 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
527 43 R 528 14 529 77 530 69 D 531 61 G	CL 14 GE	567	00 0 77 GE



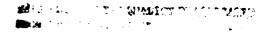
```
615
                                  94 + -
574
      14
          D
                           616
                                  55
575
      71 SBR
                           617
576
      37 P/R
                                      5
                           618
                                  05
577
      43 RCL
                           619
                                  65
                                      X
578
      14
          14
                           620
                                  43 RCL
579
      77
          GE
                           621
622
623
                                     00
580
      69 DP
                                  00
                                     +
581
      61 GTO
                                  85
                                     1
582
                                  01
      00
          00
                           624
625
583
                                  54
                                     \rightarrow
      00
          00
                                  92 RTN
584
      76 LBL
                           626
                                  76 LBL
585
      50 I×I
                           627
628
                                  59 INT
586
      53
         (
                                  02
                                     2
587
      93
         •
5
                           629
                                  44 SUM
588
      05
                           630
                                  12 12
      94 +/-
589
         ÷
6
                                  92 RTN
                           631
590
      55
                           632
                                  76 LBL
591
      06
                           633
634
                                  48 EXC
592
      05
          5
593
                                  02
                                     2
      65
         ×
594
                           635
                                  44 SUM
      43 ROL
                                  13
595
      00 00
                           636
                                     13
596
                           637
                                  92 RTN
      85
                           638
639
                                  76 LBL
597
      01
          1
                                  80 GRD
598
         )
      54
599
                           640
                                  53
      92 RTN
                                     (
                           641
                                  43 RCL
600
      76 LBL
                           642
601
      89
                                  15
                                     15
          Π
                            643
                                  55
602
      43 RCL
                           644
                                  01
603
      00
         00
                                     2
0
                           645
                                  02
604
      32 X:T
                           646
                                  00
605
      08
         8
                           647
                                     0
                                  00
606
      77
         GE
                                     )
                           648
                                  54
607
      28 LOG
                           649
                                  22 INV
608
      92 RTN
                           650
                                  44 SUM
609
      76 LBL
                           651
                                  00 00
610
      79
          \bar{X}
                           652
                                  92 RTN
      53
          ζ.
611
                           653
      93
                                  76 LBL
612
      02
                           654
                                  70 RAD
613
          5
                            655
                                  03
614
      05
```

```
Ξ
                               697
                                      15
656
      44
          SUM
                                           8
                               698
                                      12
657
      19
            19
658
                               699
                                      36
                                          PGM
      92
          RTN
                                      15
                                           15
      76
                               700
659
          LBL
                                          0.
                                      18
          NDP
                               701
660
      68
                                      32
661
                                         XIT
      06
            6
                               702
                                      00
                                           0
                               703
662
      06
            6
                                      77
                                           GE
663
      99
          PRT
                               704
                                      57
                               705
                                          ENG
      61
          GTO
664
          ₿.
                                      92
                               706
                                          RTH
665
       17
666
667
668
                                      76
                                          LBL
       76
          LBL
                                707
       97
          DSZ
                               708
                                      29
                                          CP
                                           26
                               709
                                      02
      01
            1
669
      04
            4
                               710
                                      06
670
                               711
                                          PRT
          PRT
                                      99.
       99
                               712
                                      43 FCL
           STF
671
       86
                                713
                                           00
            02
                                      00
672
       02
                                          PRI
                                714
                                      99
673
       61
           GTO
674
                                           0
                                715
                                      00
            00
       00
                                716
717
675
676
                                      42
                                          STO
       00
            00
                                           12
                                      12
       76
          LBL
       58
          FIX
                                718
                                      42
                                          STO
677
                                719
                                      13
                                           13
678
       02
            2
                                      92
679
680
            4
                                720
                                          RTN
       04
       99 PRT
                                721
                                      76
                                          LEL
                                722
                                      96
                                          WRT
       61 GTO
681
                                723
                                       43
                                          RCL
            04
682
       04
                                724
                                       17
                                            17
       10
            10
683
                                725
                                       32
                                          XIT
       76
684
          LBL
                                726
                                      08
                                            3
       57
685
           ENG
                                            GE
          PGM
                                727
                                       77
686
       36
                                728
729
                                       28
                                          LOG
687
       15
            15
                                      92
                                          RTH
688
       10 E'
                                730
                                       76
                                          LBL
 689
       43 RCL
                                731
                                       78
                                           Z+
 690
       10
            10
                                            25
                                       02
 691
       36
           PGM
                                732
                                       05
 692
       15
            15
                                733
                                       99
                                          PRT
                                734
            A
 693
       11
                                735
                                       43
                                          RCL
 694
       43
           RCL
                                       17
                                            17
 695
       11
            11
                                736
                                       99 PRT
                                737
       36
           PGM
 696
```



```
738
      OO
          ū
739
         STO
      42
      12
740
          12
741
      42
         STO
742
      13
          13
      92 RTN
743
744
      76 LBL
745
      35 1/X
746
      53
          (
747
      43 RCL
      15
           15
748
749
      55
750
751
      01
           1
           2
      02
752
      00
           Ü
753
754
      00
           0
      54
755
      22 INV
756
      44 SUM
      17
757
          17
758
      92 RTN
759
      76 LBL
760
      45 YX
          3
761
      0.3
762
      44 SUM
763
      01
          01
764
      92 RTN
      76 LBL
765
      44 SUM
766
767
      01
           1
           2
768
      02
769
770
      99 PRT
      61 GTO
771
       10 E'
772
      00
          0
773
       22 INV
       90 LST
 774
775
       98 ADV
 776
       98 ADV
           5
 777
       05
778
       00
```

```
779
      42 STD
780
      00
          - 00
781
      00
           0
782
      42 STD
      12
783
          12
      42 STD
784
      13
          13
785
      42 STD
786
      19
          19
787
      32 X:T
788
789
      01
          1
790
      22 INV
791
      44 SUM
792
793
794
          18
      18
      43 RCL
      18
           18
795
      67
           EQ
796
           07
      07
797
798
799
           99
      99
      S1 RST
      91 R/S
```



## APPENDIX B INSTRUCTION SHEET

This is a physical fitness test.

#### I. WHAT WE ARE EXAMINING AND WHY

The following tests will look at the complex systems that make up the network of health and fitness. First we will test your upper body endurance and muscular strength. Next we will examine your cardiovascular health. This test is a component of a research project being conducted by graduate students of the Naval Postgraduate School.

#### II. MUSCULAR ENDURANCE AND STRENGTH

Muscular endurance is often synonymously and incorrectly used in place of muscular strength. Muscular strength is the ability of your muscular system to exert maximum force against an object or resistance all at once, your ability to exert a maximum force a single time.

Muscular endurance relates to the ability to exert force, not necessarily maximal, over an extended time period. As with all the components of fitness, these two concepts are interrelated but distinctly different from each other. Each concerns itself with particular capacities of fitness.

#### III. CARDIOVASCULAR HEALTH

Objective: To measure your heart-rate response to exercise. This test will determine the relative efficiency of your heart and circulatory system. Your heart rate can be used to describe the fitness level of your body in three areas: how much oxygen you need, how much blood

TABLE B-1.1

your heart must pump to supply this need, and how hard your heart must work at this task. If your need for oxygen is not being fulfilled, your body is working in an inefficient manner. Consequently, more blood will have to be pumped through your circulatory system at a faster rate to get the oxygen to the muscles and organs that need it. The heart has the responsibility of satisfying your body's need for oxygen. It will have to beat more frequently to circulate the blood throughout your system. If your body works in an efficient manner, its need for oxygen is being fulfilled.

Thus cardiovascular health relates to the ability of the heart, lungs, and blood vessels to work in unison without strain. Regardless of what the task is, whether physical or mental, the cardiovascular system should be able to handle it. When you have high levels of cardiovascular health you perform with more efficiency and you are more effective at what you do.

#### QUESTIONNA IRE

### THIS IS A PHYSICAL FITNESS TEST READ THIS DOCUMENT CAREFULLY BEFORE THIS TEST BEGINS

- (1) This test is completely voluntary! You may decline testing now if you wish. You may stop at any time during this test and decline further testing. You are under no obligation to complete this test.
- (2) Before proceeding with this test, you should assure yourself and your tester that there have been no incidents in your medical history that would prohibit you from pursuing this testing. Your medical history is relevant to this physical fitness test.
- (3) Please answer the following statements: YES or NO
  - (a) I have a heart related disease.
  - (b) I have high blood pressure.
  - (c) I often feel faint and suffer spells of dizziness.
  - (d) I have recently or in the past felt pain, heaviness or pressure in my chest.
  - (e) I have felt pain, heaviness or pressure in my chest when I walk uphill.
  - (f) My doctor has advised me not to engage in physical exercise or physical activity.
- (4) I have read and fully understand this document.

DATE	C T CMA (PLTOE)
DAIL	SIGNATURE
<del></del>	

#### DATA SHEET

NA ME				<del></del>			
AGE	WEIGHT			DATE	<u> </u>	<del></del>	
PHYSICAL ACTIVITY CA	TEGORY:	I	II	III	IA	Λ	VI
STRENGTH TEST:	Maximu Maximu			ss			
ENDURANCE TEST:	Bench :	Press	Repet	itions W	ith 1	.00 Pc	ounds
	Curl R	epeti <sup>.</sup>	tions	With 55	Pound	ls	
CARDIOVASCULAR TEST:	(Pulse : Restin						
	Immedi	ate P	ost Ex	ercise			
	30 Sec	onds :	Post E	xercise			<del></del>
	60 Sec	onds :	Post E	xercise			
	<b>1</b> 20 Se	conds	Post	Exercise			

Code	Score					
	-	18		140	132	132
	7	96	152	136 140		
	n	92	148	132	124 128	120 124 128
	4	88	144	128	120	120
	S	22	136 140 144 148	124	112 116 120	116
	9	80	136	120		112 116
	7	78	132	112 116 120 124 128	. 108	
	∞ .	92.	104 108 112 116 120 124 128 132	112	100	100 104 108
	0	74	124	108	18	91
Sa	10	22	120	102	%	%
Codes	11	20	116	96 100 104	92	92
	12	88	112		88	88
	13	99	108	. 22	84	22
	14	22	104	88	80	80
	15	62	100	2	26	92
	16	8	%	8	8	2
	17	55	. 2		89	<u> </u>
	18	52	88	8	2	2
	19	43	ಪ	- 3	. 8	99
	20	44	80	2	32	አ
		Resting Hoart Rate	Posttest Heart Rate	Second Recovery Heart Rate	1 Minute Recovery Heart Rate	2 Minute Recovery Heart Rate

Total Code Score

TABLE B-4

#### CATEGORY I RESULTS

SUBJECT	ACE	WEIGHT	CARDIOVASCULAR SCORE (1)	STRENCTH SCORE (2)	ENDURANCE SCORE (3)
1	29	190	56.5	1.26	24.1
2	33	155	58.0	1.32	12.9
3	36	170	58.0	•97	5.5
4	31	205	44.5	1.19	27.9
5	37	157	33.5	1.13	10.1
6	34	160	40.0	1.16	11.0

See Table B-17 for derivation
 See Table B-18 for derivation
 See Table B-19 for derivation

#### CATECORY II RESULTS

SUBJECT	AGE	WEIGHT	CARDIOVASCULAR SCORE (1)	STRENGTH SCORE (2)	ENDURANCE SCORE (3)
1	33	167	91.5	1.47	22.0
2	34	195	96.5	1.41	28.9
3	35	180	55 <b>.</b> 0	1.11	12.2
L <sub>+</sub>	33	160	93•5	1.44	13.6
5	28	127	82.0	1.34	6.5
6	30	158	82.0	1.11	6.6

See Table B-20 for derivation
 See Table B-21 for derivation
 See Table B-22 for derivation

#### CATEGORY III RESULTS

SUBJECT	AGE	WEIGHT	CARDIOVASCULAR SCORE (1)	STRENGTH SCORE (2)	ENDURANCE SCORE (3)
1	22	200	35.0	2.48	50.0
2	23	202	56.0	2.35	62.5
3	28	205	44.5	2.49	37.2
4	34	220	86.5	2.23	42.7
5	25	180	67.0	2.83	54.8
6	29	225	24.5	2.00	1.6ر

<sup>(1)</sup> See Table B-23 for derivation(2) See Table B-24 for derivation(3) See Table B-25 for derivation

#### CATEGORY IV RESULTS

SUBJECT	AGE	WEICHT	CARDIOVASCULAR SCORE (1)	STRENGTH SCORE (2)	ENDURANCE SCORE (3)
1	28	200	96.5	2.30	47.5
2	31	180	79.0	2.67	49.0
3	32	<b>1</b> 65	85.0	2.00	43.7
4	32	<b>1</b> 60	79.0	2.19	47.2
5	19	240	89 <b>.</b> 5	1.85	34.3
6	26	180	71.5	2.39	44.6

See Table B-26 for derivation
 See Table B-27 for derivation
 See Table B-28 for derivation

#### CATECORY V RESULTS

SUBJECT	AGE	WEIGHT	CARDIOVASCULAR SCORE (1)	STRENGTH SCORE (2)	ENDURANCE SCORE (3)
1	30	165	39.5	2.03	25.5
2	24	175	55.0	2.43	54•1
3	19	185	47.0	1.86	47.0
4	34	179	77.5	1.73	33.5
5	35	205	59•5	1.15	22.0
6	30	120	56.5	1.75	23.8

See Table B-29 for derivation
 See Table B-30 for derivation
 See Table B-31 for derivation

#### CATEGORY VI RESULTS

SUBJECT	ACE	WEIGHT	CARDIOVASCULAR SCORE (1)	STRENGTH SCORE (2)	ENDURANCE SCORE (3)
1	27	<b>1</b> 80	61.0	1.42	23.1
2	32	<b>12</b> 5	47.5	1.56	17.4
3	31	170	65.5	1.26	14.7
4	31	<b>1</b> 70	85.0	1.41	15.3
5	33	175	86.5	1.34	11.4
ó	30	205	30.0	1.15	17.9

<sup>(1)</sup> See Table B-32 for derivation (2) See Table B-33 for derivation (3, See Table B-34 for derivation

Univariate User Instructions						
Step	Procedure	Enter	Press	Display		
1.	Initialize		2nd E'	31		
2.	Enter data	× <sub>i</sub>	A	i		
	Repeat for each x					
3.	Recall Statistics		2nd ₹	x		
			INV 2nd R	s		
			2nd OP 11	MSD		
			RCL 12	x <sub>min</sub>		
1			RCL 13	x <sub>max</sub>		
			RCL 14	MIDVAL		
			RCL 15	range		
			2nd A'	MAD		
			RCL 03	n		
4.	Recall data entered in					
	Step 2 if desired.		RCL 31	×1		
}			RCL 32	<b>x</b> <sub>2</sub>		
			RCL 31 + i -1	x <sub>i</sub>		
			<u> </u>			

TABLE B-11

#### UNIVARIATE PROGRAM

```
000
     76 LBL
                          041
                               18 C.
     10 E'
001
                          042
                               22 INV
     47 CMS
002
                          043
                               77
                                   GE
     22 INV
003
                          044
                               00 00
     86 STF
004
                         045
                               57
                                  57
005
     00 00
                         046
                               43 RCL
006
     03 3
                         047
                               13
                                  13
     01 1
007
                         048
                               32 X:T
008
     42 STO
                         049
                               43 RCL
009
     30 30
                         050
                               18 18
010
     91 R/S
                         051
                               77
                                   GΕ
011
     76 LBL
                         052
                               00 00
012
     11
        Ħ
                         053
                               62
                                   62
013
     42 STO
                         054
                               61 GTO
014
     18 18
                         055
                               00
                                  00
015
     72 ST*
                         056
                               64
                                   64
016
     30 30
                         057
                               42 STD
017
     01
        1
                         058
                               12
                                  12
     44 SUM
018
                         059
                               61 GTD
019
     30 30
                         060
                               00 00
020
     87 IFF
                         061
                               64 64
021
     00 00
                         062
                               42 STO
022
     65 ×
                         063
                              13 13
023
     43 RCL
                         064
                               53 (
024
     18
        18
                               53 (
                         065
025
     42 STO
                         066
                               43 ROL
     12 12
026
                              12 12
85 +
                         067
027
     42 STO
                         068
028
     13 13
                         069
                               43 RCL
     78 X+
029
                         070
                               13 13
     86 STF
030
                         071
                               54
     00 00
031
                         072
                               55 ÷
                              02 2
54 )
032
     43 RCL
                         073
033
     03 03
                         074
     91 R/S
034
                              42 STO
                         075
035
     76 LBL
                         076
                               14 14
036
     65 ×
                         077
                              53 🦿
037
     43 RCL
                         078
                               43 ROL
038
     12 12
                         079
                               13 13
039
     32 X1T
                              75
                         080
    43 RCL
040
                         081
                              43 ROL
           TABLE B-12.1
```

131

```
082
       12
                                 124
                                        07
083
                                125
126
127
       54
            )
                                            SUN
                                        44
084
       42
          STO
                                        43
                                            43
           15
       15
085
                                        19 D°
55 ÷
086
       43 RCL
                                 128
087
           13
                                 129
130
       18
                                        43 RCL
088
       61 GTO
                                        03
                                            -03
                                131
132
133
134
135
136
137
089
       00
          0.0
                                        95
                                            =
090
       29
          29
                                        91 R/S
091
       76 LBL
                                        76 LBL
092
093
       16 A'
                                        14 D
      79 %
94 +/- %
10 STO
                                            3
                                        03
094
                                            1
                                        01
095
                                        42 STD
096
       16
                                138
                                        30
                                            30
       43 RCL
03 03
097
                                139
                                        91 R/S
098
099
                                140
                                        00
                                            Ū
       42 STD
                                 141
                                        00
                                            - 0
      07 07
03 3
100
                                 142
                                        00
                                            101
                                143
144
                                             Û
                                        00
102
       01
          1
                                        00
                                             Ũ
103
104
      42 STB.
                                145
146
                                        00
                                             20 20
                                        00
                                             0
105
       00 0
                                147
                                        00
                                             0
106
107
       42 STD
                                148
                                        00
                                             Ü
       19- 19
                                149
                                        00
                                             Ð
108
109
110
       76 LBL
                                 150
                                        00
                                             0
                                151
152
153
       44 SUM
                                        00
                                             0
       53 (
                                        00
                                             0
111
112
       73 RC*
                                        00
                                             0
       20
           20
                                 154
                                             0
                                        OQ.
113
       85
           +
                                             O
                                 155
                                        00
114
115
       43 RCL
                                156
157
                                        00
                                             0
       16
           16
                                        ŨŨ
                                             0
116
       54
           · >
                                 158
                                        00
                                             0
117
       50; I×I
                                159
                                        00
                                             0
118
       44' SUM
                                160
                                        00
                                             0
119
120
121
           19
       19
                                 161
                                        00
                                             0
          - 1
       01
                                 162
                                        00
                                             \mathbf{0}
       44 SUM
                                 163
                                        00
122
       20
          20 ..
```

TABLE B-12.2

	ANOVA USER IN	STRUCTIONS		
Step	Procedure	Enter	Press	Display
1	Select Program 06		2nd Pgm 06	
2	Initialize data base		2nd E'	0
3	Enter data for each row	x <sub>ij</sub>	A	ri
īτ	Reset pointer if more than 29 data entries are made		ם	31
5	Calculate x for current		2nd B'	x <sub>i</sub>
6	Calculate MSD for current row		2nd C'	MSD <sub>i</sub>
7	Return to step 3 to enter next row data			
8	Return pointer to ANOVA program		RST	
9	Calculate ANOVA table entries Note: the numbers in parentheses in the		A R/S	ss <sub>r</sub> (1) r-1 (2)
	display column correspond to the		R/S	MSS <sub>r</sub> (3)
	numbered blocks in the ANOVA table		R/S	ss <sub>u</sub> (4)
	(table 4-4)	,	R/S	r(n-1) (5)
			R/S	MSS <sub>u</sub> (6)
			R/S	ss <sub>t</sub> (7)
			R/S	(nr-1) (8)
			R/S	F ratio (9)
			R/S	Prob-value (10)

TABLE B-13.1

	ANOVA USER	INSTRUCTIONS		
Step	Procedure	Enter	Press	Display
	Confidence Intervals fo	r		
10	Initialize		E'	0
11	Enter contrast data	c <sub>i</sub>	R/S	c <sub>i</sub>
	Repeat for each row i	× <sub>i</sub>	R/S	×i
		n <sub>i</sub>	R/S	n <sub>i</sub>
12	Enter F percentile with degrees of freedom r-1, r(n-1)	F	A' x <b>Z</b> t	1 µ

TABLE B-13.2

#### ANOVA PROGRAM

001 002 003 004 005 006 007 008 009 010 011	76 LBL 11 A 36 PGM 15 15 11 A 42 STD 00 RCL 08 R/S 43 RCL 14 14 91 R/S 43 RCL		032 033 034 035 036 037 038 040 041 042 044 044	75 1 95 2 91 7 91 7 91 7 91 8 91 8 91 8 91 8 91 8 91 8 91 8 91 8
006 007 008 009 010	00 00 43 RCL 08 08 91 R/S		038 039 040 041 042 043 044	91 R/8 43 RCL 14 14 36 PGM 22 22 11 A

```
064
       42 STO
                                  095
                                        65
                                            \times
065
       01
          01
                                  096
                                        43 RCL
066
067
       91 R/S
                                  097
                                        14
                                             14
       42 STO
                                  098
                                        65
                                             \times
                                        43 RCL
068
       02
          02
                                  099
069
070
071
       91 R/S
                                  100
                                        29
                                            29
       35 1/%
                                 101
                                        65
                                            X
       65
          ×
                                 102
                                        43 RCL
072
073
074
       43 RCL
                                 103
                                        03
                                            03
       01 01
                                 104
                                        95 =
       33 X2
                                 105
                                        34 IX
075
076
077
                                        42 STO
       95
          =
                                 106
       44 SUM
                                 107
                                        05
                                            05
                                 108
109
       03 03
                                        85
078
079
080
       43 RCL
                                        43 RCL
                                 110
       01
           01
                                        06
                                            - 06
                                        95 =
32 X:T
                                 111
       65
          ×
081
082
083
                                 112
113
       43 RCL
       02
           02
                                        43 RCL
       95
           =
                                 114
115
                                        06 06
084
085
       44 SUM
                                        75
                                 116
117
118
       06 06
                                        43 ROL
086
       01
           1
                                        05 05
087
       44 SUM
                                        95
088
           0^{A}
                                 119
       04
                                        92 RTN
                                 120
121
122
089
       43 RCL
                                        00
                                             0
090
091
       04
           04
                                        00
                                             Ū
       61 GTO
                                        00
                                             Ū
092
                                 123
       33 X2
                                        00
      76 LBL
093
                                 124
                                        00
                                             0
       16 A'
094
                                 125
                                       00
```

# DECREES OF FREEDOM

PROB-VALUE

 $\frac{100}{x}$ 

(r-1)

 $\begin{array}{ccc}
\mathbf{r} & \mathbf{r} \\
\mathbf{n} & \mathbf{\Sigma} & (\bar{\mathbf{x}}_{\mathbf{i}} - \bar{\mathbf{x}})^2 \\
\mathbf{1} = \mathbf{1}
\end{array}$ 

BETWEEN ROWS

(C)

(2)

9

 $\begin{array}{ccc} \mathbf{r} & \mathbf{n} \\ \Sigma & \Sigma \\ \mathbf{i} & \mathbf{j} \end{array} (\mathbf{x_{i,j}} - \bar{\mathbf{x}_{i}})^{2} & \mathbf{r}(\mathbf{n} - \mathbf{1}) \end{array}$ 

WITHIN ROWS

6

(J

**(** 

$$(nr - 1)$$

 $\sum_{i} \sum_{j} (x_{i,j} - \bar{x})^{2}$ 

TOTAL

TABLE B-15

# FITNESS EXAMPLE

SUBJECT

~

 $\sim$ 

5

9

CATEGORY

I (Sedentary)

 $^{\rm x}_{\rm I1}$ 

 $x_{II3}$ 

x<sub>III5</sub>

 $\bar{x}_{\rm III}$ 

 $\bar{x}_{\rm II}$ 

ıΫ́

 $\bar{\mathbf{x}}_{\mathbf{j}} = \frac{1}{n_{\mathbf{j}}} \sum_{\mathbf{j}} \mathbf{x}_{\mathbf{j},\mathbf{j}}$ 

n<sub>i</sub> = the number of subjects
 in Category i

 $\ddot{\mathbf{x}} = \frac{1}{r} \quad \overset{\mathbf{r}}{\Sigma} \quad \ddot{\mathbf{x_1}}$   $\mathbf{i} = 1 \quad \mathbf{i}$ 

r = the number of categories

TABLE B-16

II (Runners)

III (Weightlifters)

CATECORY I - CARDIOVASCULAR SCORES

	Resting	Immediate	30 Sec	oes 09	120 Sec	Score
Subject #1 - Heart Rate Pipes Score	66	114	108	90	90	56.5
Subject #2 - Heart Rate Pipes Score	72 10	114	96 12	90 11.5	84 13	58
Subject #3 - Heart Rate Pipes Score	66 13	126 8.5	102 10.5	90	78 14.5	58
Subject #4 - Heart Rate Pipes Score	78 7	120 10	108 9	102 8.5	96 10	5.44
Subject #5 - Heart Rate Pipes Score	84 5	132	114	108	108	33.5
Subject #6 - Heart Rate Pipes Score	78	126 8.5	114	102 8.5	102 8.5	017

TABLE B-17

#### CATEGORY I - ADJUSTED STRENGTH SCORES

$$S_{11} = \frac{150 + 90}{190} = 1.26$$

$$s_{12} = \frac{130 + 75}{155} = 1.32$$

$$s_{13} = \frac{90 + 75}{170} = .97$$

$$s_{14} = \frac{160 + 85}{205} = 1.19$$

$$s_{15} = \frac{105 + 70}{157} = 1.13$$

$$s_{16} = \frac{110 + 75}{160} = 1.16$$

$$S_{1\bar{x}} = \frac{124 + 78}{173} = 1.17$$

#### CATEGORY I - ADJUSTED ENDURANCE SCORES

$$E_{11} = (\frac{100}{BODY \text{ WT}}) (\frac{\text{NUMBER OF BENCH PRESS}}{\text{REPETITIONS}}) + (\frac{55}{BODY \text{ WT}}) (\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}})$$

$$E_{11} = (\frac{100}{190}) (31) + (\frac{55}{190}) (27) = 24.1$$

$$E_{12} = (\frac{100}{155}) (9) + (\frac{55}{155}) (20) = 12.9$$

$$E_{13} = (\frac{100}{170}) (0) + (\frac{55}{170}) (17) = 5.5$$

$$E_{14} = (\frac{100}{205}) (32) + (\frac{55}{205}) (46) = 27.9$$

$$E_{15} = (\frac{100}{157}) (2) + (\frac{55}{157}) (25) = 10.1$$

$$E_{16} = (\frac{100}{160}) (5) + (\frac{55}{160}) (23) = 11.0$$

$$E_{1\bar{x}} = (\frac{100}{173}) (13) + (\frac{55}{173}) (26) = 15.7$$

CATECORY II - CARDIOVASCULAR SCORES

	Resting	Inmediate	30 Sec	60 Sec	120 Sec	Score
Subject #1 - Heart Rate Pipes Score	60 16	90	60 20	60	60 19	91.5
Subject #2 - Heart Rate Pipes Score	448 119	90	60	748 70 70	48 20	5.96
Subject #3 - Heart Rate Pipes Score	72 10	120 10	102 10.5	96 10	78 14.5	55.0
Subject #4 - Heart Rate Pipes Score	54 17.5	900	66 19.5	60	54 20	93.5
Subject #5 - Heart Rate Pipes Score	66 13	90	72 18	72 16	66 17.5	82
Subject #6 - Heart Rate Pipes Score	60 16	108 13	72 18	66 17.5	66 17.5	82

TABLE B-20

## CATEGORY II - ADJUSTED STRENGTH SCORES

$$S_{21} = \frac{BENCH PRESS + CURL}{BODY WEIGHT}$$

$$S_{21} = \frac{160 + 85}{167} = 1.47$$

$$S_{22} = \frac{170 + 105}{195} = 1.41$$

$$s_{23} = \frac{130 + 70}{180} = 1.11$$

$$s_{24} = \frac{150 + 80}{160} = 1.44$$

$$S_{25} = \frac{110 + 60}{127} = 1.34$$

$$s_{26} = \frac{100 + 75}{158} = 1.11$$

$$S_{2\bar{x}} = \frac{137 + 79}{165} = 1.31$$

#### CATEGORY II - ADJUSTED ENDURANCE SCORES

$$E_{21} = (\frac{100}{BODY \text{ WT}}) (\frac{\text{NUMBER OF BENCH PRESS}}{\text{REPETITIONS}}) + (\frac{55}{BODY \text{ WT}}) (\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}})$$

$$E_{21} = (\frac{100}{167}) (23) + (\frac{55}{167}) (25) = 22.0$$

$$E_{22} = (\frac{100}{195})(31) + (\frac{55}{195})(46) = 28.9$$

$$E_{23} = (\frac{100}{180}) (11) + (\frac{55}{180}) (20) = 12.2$$

$$E_{24} = (\frac{100}{160}) (14) + (\frac{55}{160}) (15) = 13.6$$

$$E_{25} = (\frac{100}{127})$$
 (5)  $+ (\frac{55}{127})$  (6)  $= 6.5$ 

$$E_{26} = (\frac{100}{158})$$
 (4) +  $(\frac{55}{158})$  (12) = 6.6

$$E_{2\bar{x}} = (\frac{100}{165}) (15) + (\frac{55}{165}) (21) = 16.1$$

TABLE B-23

	Resting	Immediate	30 Sec	eo Sec	120 Sec	Scure
Subject #1 - Heart Rate Pipes Score	90 3.5	120 10	120 Č	102 8.5	001 C	3,5
Subject #2 - Heart Rate Pipes Score	% % %	114	114	46 10	96 10	56.
ate Score	7R 7	120 10	114	96 10	96 10	5.44.5
Rate Score	54 17.5	17.5	15	17.5	60 19	86.5
Rate Score	72 10	114	78 16.5	78 14.5	23 14.5	<i>L</i> 9
Rate Score	84	138 5.5	132 3	120 4	108	24.5

CATECORY III - CARDIOVASCULAR SCORES

## CATEGORY III - ADJUSTED STRENGTH SCORES

$$s_{3i} = \frac{BENCH \ PRESS + CURL}{BODY \ WEIGHT}$$

$$s_{3i} = \frac{330 + 165}{200} = 2.48$$

$$s_{32} = \frac{320 + 155}{202} = 2.35$$

$$s_{33} = \frac{375 + 135}{205} = 2.49$$

$$s_{34} = \frac{305 + 185}{220} = 2.23$$

$$s_{35} = \frac{320 + 190}{180} = 2.83$$

$$s_{36} = \frac{320 + 130}{225} = 2.00$$

$$s_{3\bar{x}} = \frac{328 + 160}{205} = 2.38$$

CATEGORY III - ADJUSTED ENDURANCE SCORES

$$E_{31} = (\frac{100}{BODY \text{ WT}}) \text{ (NUMBER OF BENCH PRESS)} + (\frac{55}{BODY \text{ WT}}) \text{ (NUMBER OF CURL)}$$

$$E_{31} = (\frac{100}{200}) (67) + (\frac{55}{200}) (60) = 50.0$$

$$E_{32} = (\frac{100}{202})(85) + (\frac{55}{202})(75) = 62.5$$

$$\mathbb{E}_{33} = (\frac{100}{205})(57) + (\frac{55}{205})(35) = 37.2$$

$$E_{34} = (\frac{100}{220}) (61) + (\frac{55}{220}) (60) = 42.7$$

$$E_{35} = (\frac{100}{180}) (70) + (\frac{55}{180}) (52) = 54.8$$

$$E_{36} = (\frac{100}{225})(54) + (\frac{55}{225})(31) = 31.6$$

$$\mathbb{E}_{3\tilde{\mathbf{x}}} = (\frac{100}{205}) (66) + (\frac{55}{205}) (52) = 46.1$$

CATECORY IV - CARDIOVASCUIAR SCORES

120 Sec Sc	20 96.5	66 17.5 79		60 19 66 17.5	60 19 66 17.5 19
oo sec	19	66	66	66 17.5 66 17.5	66 17.5 66 17.5 19
30 Sec	19.5	72 18	72 18	72 18 72 18	72 18 72 18 18
Immediate	19	108 13	102 14.5	102 14.5 108 13	102 14.5 108 13 90 17.5
Kesting	440 19	66 13	60 16	60 16 66 13	60 66 13 13 16
	Subject #1 - Heart Kate Pipes Score	Subject #2 - Heart Rate Fipes Score	Subject #3 - Heart Rate Pipes Score	Subject #3 - Heart Rate Pipes Score Subject #4 - Heart Rate Fipes Score	

## CATECORY IV - ADJUSTED STRENGTH SCORES

$$S_{4i} = \frac{BENCH PRESS + CURL}{BODY WEIGHT}$$
 $S_{41} = \frac{290 + 170}{200} = 2.30$ 
 $S_{42} = \frac{305 + 175}{180} = 2.67$ 
 $S_{43} = \frac{205 + 125}{165} = 2.00$ 
 $S_{44} = \frac{230 + 120}{160} = 2.19$ 
 $S_{45} = \frac{310 + 135}{240} = 1.85$ 
 $S_{46} = \frac{275 + 155}{180} = 2.39$ 

 $S_{4\bar{x}} = \frac{270 + 147}{188} = 2.22$ 

# CATEGORY IV - ADJUSTED ENDURANCE SCORES

$$E_{\downarrow\downarrow\downarrow} = (\frac{100}{\text{BODY WT}}) (\frac{\text{NUMBER OF BENCH FRESS}}{\text{REPETITIONS}}) + (\frac{55}{\text{BODY WT}}) (\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}})$$

$$E_{41} = (\frac{100}{200}) (52) + (\frac{55}{200}) (78) = 47.5$$

$$\Xi_{42} = (\frac{100}{150})(53) + (\frac{55}{180})(64) = 49.0$$

$$\Xi_{43} = (\frac{100}{155})(44) + (\frac{55}{165})(51) = 43.7$$

$$E_{0.0} = (\frac{100}{160})(37) + (\frac{55}{160})(70) = 47.2$$

$$E_{45} = (\frac{100}{240})(55) + (\frac{55}{240})(50) = 34.3$$

$$E_{46} = (\frac{100}{180}) (50) + (\frac{55}{180}) (55) = 44.6$$

$$E_{4\bar{x}} = (\frac{100}{188}) (49) + (\frac{55}{188}) (61) = 43.9$$

CATECORY V - CARDIOVASCUIAR SCORES

Score	39.5	55	24	77.5	59.5	56.5
120 Sec	96 10	90	90	66 17.5	78 14.5	78 14.5
60 Sec	102 8.5	90	90	72 16	84 13	90 11.5
30 Sec	108 9	102 10.5	96	78 16.5	102 10.5	90
Immediate	132	11 <sup>4</sup> 11.5	126 8.5	102 14.5	126 8.5	120 10
Resting	48 5	72 10	90 3.5	66	66 13	78
	Subject #1 - Heart Rate Pipes Score	Subject #2 - Heart Rate Fipes Score	Subject #3 - Heart Rate Fipes Score	Subject #4 - Heart Rate Pipes Score	Subject #5 - Heart Rate Pipes Score	Subject #6 - Heart Rate Pipes Score

TABLE B-29

## CATECORY V - ADJUSTED STRENGTH SCORES

$$S_{5i} = \frac{\text{BENCH PRESS} + \text{CURL}}{\text{BODY WEIGHT}}$$

$$S_{51} = \frac{220 + 115}{165} = 2.03$$

$$S_{52} = \frac{265 + 160}{175} = 2.43$$

$$S_{53} = \frac{220 + 125}{185} = 1.86$$

$$S_{54} = \frac{200 + 110}{179} = 1.73$$

$$S_{55} = \frac{170 + 65}{205} = 1.15$$

$$S_{56} = \frac{140 + 70}{120} = 1.75$$

$$S_{5\bar{x}} = \frac{203 + 108}{172} = 1.81$$

#### CATEGORY V - ADJUSTED ENDURANCE SCORES

$$E_{51} = (\frac{100}{BODY \text{ WT}}) \text{ (NUMBER OF BENCH PRESS)} + (\frac{55}{BODY \text{ WT}}) \text{ (NUMBER OF CURL)}$$

$$E_{51} = (\frac{100}{165}) (30) + (\frac{55}{165}) (22) = 25.5$$

$$E_{52} = (\frac{100}{175}) (37) + (\frac{55}{175}) (105) = 54.1$$

$$E_{53} = (\frac{100}{185}) (54) + (\frac{55}{185}) (60) = 47.0$$

$$E_{54} = (\frac{100}{179}) (33) + (\frac{55}{179}) (49) = 33.5$$

$$E_{55} = (\frac{100}{205}) (28) + (\frac{55}{205}) (31) = 22.0$$

$$E_{56} = (\frac{100}{120}) (22) + (\frac{55}{120}) (12) = 23.8$$

$$E_{5\bar{x}} = (\frac{100}{172}) (34) + (\frac{55}{172}) (47) = 34.8$$

CATECORY VI - CARDIOVASCULAR SCORES

Score	61	47.5	65.5	85	86.5	80
120 Sec	78 14.5	90	72 16	60	66 17.5	60
60 Sec	84 13	90	78 14.5	66 17.5	66 17.5	84 13
30 Sec	96	108 9	90	72 18	78 16.5	90 13.5
Immediate	114 11.5	126 8.5	114	102 14.5	70 17.5	102 14.5
Resting	72 10	78	72 10	60 16	54 17.5	42 20
	Subject #1 - Heart Rate Pipes Score	Subject #2 - Heart Rate Pipes Score	Subject #3 - Heart Rate Pipes Score	Subject #4 - Heart Rate Pipes Score	Subject #5 - Heart Rate Pipes Score	Subject #6 - Heart Rate Pipes Score

TABLE B-32

### CATEGORY VI - ADJUSTED STRENGTH SCORES

$$s_{6i} = \frac{BENCH PRESS + CURL}{BODY WEIGHT}$$

$$s_{61} = \frac{155 + 100}{180} = 1.42$$

$$s_{62} = \frac{120 + 75}{125} = 1.56$$

$$s_{63} = \frac{130 + 85}{170} = 1.26$$

$$s_{64} = \frac{135 + 105}{170} = 1.41$$

$$s_{65} = \frac{145 + 90}{175} = 1.34$$

$$s_{66} = \frac{145 + 90}{205} = 1.15$$

$$S_{6\bar{x}} = \frac{138 + 91}{171} = 1.34$$

#### CATEGORY VI - ADJUSTED ENDURANCE SCORES

$$E_{6i} = (\frac{100}{BODY \text{ WT}}) (\frac{\text{NUMBER OF BENCH PRESS}}{\text{REPETITIONS}}) + (\frac{55}{BODY \text{ WT}}) (\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}})$$

$$E_{61} = (\frac{100}{180}) (25) + (\frac{55}{180}) (30) = 23.1$$

$$E_{62} = (\frac{100}{125}) (14) + (\frac{55}{125}) (14) = 17.4$$

$$E_{63} = (\frac{100}{170}) (14) + (\frac{55}{170}) (20) = 14.7$$

$$E_{64} = (\frac{100}{170}) (15) + (\frac{55}{170}) (20) = 15.3$$

$$E_{65} = (\frac{100}{175}) (10) + (\frac{55}{175}) (18) = 11.4$$

$$E_{66} = (\frac{100}{205}) (23) + (\frac{55}{205}) (25) = 17.9$$

$$E_{6\bar{x}} = (\frac{100}{171}) (17) + (\frac{55}{171}) (21) = 16.8$$

	SUBJECT #1	#2	#3	†1#	#5	9#	ı×
CATECORY							
	86.5	58.0	58.0	5.44	33.5	0.04	<b>1.84</b>
Ξ	91.5	96.5	55.0	93.5	82.0	82.0	83.4
111	35.0	56.0	0. 414	86.5	0.79	24.5	52.2
1 V	96.5	79.0	85.0	79.0	89.5	71.5	83.4
<b>.</b>	39.5	55.0	0.74	77.5	59.5	56.5	55.8
ΙΛ	61.0	47.5	65.5	85.0	86.5	80.0	70.9

1×	1.17		1.31	(	2.39	600	(u)	1,83		1.36
9#	1.16		1.11		2.00	6	66.7		()•1	1.15
5#	1.13		1.34		2.83	•	70.1	\ *	(1.1)	1.34
47#	140	4	1,44		2.23	(	2.19		1.73	1.41
#3	S		1.11		5.49		2.00		1.86	1.26
#2	°°	1.)&	1,41		2.35	,	2.67		2,43	1.56
SUBJECT #1	,	1.20	1.47		2.48		2,30		2.03	1.42
	CATECORY	<b>⊢</b> √	II		III		IV		۸	VI

١×		15.25	14.90	46.46	44.38	34.32	16.63
9#		11.0	9.9	31.6	9.177	23.8	17.9
4,5		10.1	6.5	54.8	34.3	22.0	11.4
41#		27.9	13.6	42.7	47.2	33.5	15.3
#3		5.5	12.2	37.2	43.7	0.54	14.7
#2		12.9	28.9	62.5	0.64	54.1	17.4
SUBJECT #1		24.1	22.0	50.0	47.5	25.5	23.1
	CATECORY	I	II	III	IV	>	١٧

#### LIST OF REFERENCES

- 1. Army, Department of, Headquarters, FM 44-90, Washington, 1977.
- 2. Army, Department of, Headquarters, Review of Selected Army Models, Washington, 1977.
- Astrand, Per-Olof and Rodahl, Kaare, <u>Textbook and Work Physiology</u>, Los Angeles: McGraw-Hill, 1978.
- 4. Barton, R. F., A Primer on Simulation and Gaming, p. 1-172, Prentice-Hall, 1970.
- Braverman, J. D., Probability, Logic, and Management Decisions, p. 80-99, McGraw-Hill, 1972.
- 6. Kovach, L.D., Computer-Oriented Mathematics, p. 69-76, Holden-Day, 1964.
- 7. McCormick, Ernest, J., Human Factors in Engineering and Design, New York: McGraw-Hill, 1976.
- 8. Meredith, J. R. and Turban, E., <u>Fundamentals of Management Science</u>, p. 455-460, Business Publications, 1977.
- 9. Pipes, Thomas V., and Vodak, Paul A., The Pipes Fitness Test and Prescription, Los Angeles: J.P. Tarcher, 1978.
- 10. Texas Instruments, Programmable 58/59 Applied Statistics Library, 1977.
- 11. Texas Instruments, Programmable 58/59 Master Library, p. 52-54, 1977.
- 12. Texas Instruments, Personal Programming (A complete Owner's Manual for TI Programmable 58/59), 1977.
- 13. Wonnacott, R. J., and Wonnacott, T. H., Introductory Statistics, New York, John Wiley, 1977.
- 14. Zehna, P. W., Calculator Statistics: A TI 59 Supplement to Wonnacott and Wonnacott, Naval Postgraduate School, 1980.

## INITIAL DISTRIBUTION LIST

		No. Copies
1.	Defense Technical Information Center Cameron Station Alexandria, Virginia 22314	2
2.	Library, Code 0142 Naval Postgraduate School Monterey, California 93940	2
3.	Defense Logistics Studies Information Exchange U.S. Army Logistics Management Center Fort Lee, Virginia 23801	1
Ÿ.	Department Chairman, Code 54 Department of Administrative Science Naval Postgraduate School Monterey, California 93940	1
5.	Professor P. W. Zehna, Code 55 Ze (thesis advisor) Department of Operations Research Naval Postgraduate School Monterey, California 93940	1
ó.	Asst. Professor R. G. Nickerson, Code 54 No Department of Administrative Science Naval Postgraduate School Monterey, California 93940	1
7.	Asst. Professor D. E. Neil, Code 55 Ne Department of Operations Research Naval Postgraduate School Monterey, California 93940	1
8.	CPT. George R. Nelson (author) 1407 Western Street Leavenworth, Kansas 66048	1
9.	CPT. Edgar E. Stanton (author) 10301 Pond Spice Terrace Burke, Virginia 22015	1
10.	CPT. James B. Allison 320 Girard Leavenworth, Kansas 66048	2

